

WILMOT EMPLOYMENT LANDS INDUSTRIAL SUBDIVISION

Hydrogeological Investigation

Project Location:

Part of Lot 20 North of Bleam's Road & Part of Lot 20 South of Snyder's Road and, Part Lot 19 North Bleams Road North of Highway 7 & 8 & Part Lot 19 South of Snyder's Road as 768957 Township of Wilmot

Prepared for:

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1.0 INTRODUCTION

1.1 Overview

MTE Consultants Inc. (MTE) was retained by Badenview Developments Inc. and New HamburgIrs Inc. to conduct a hydrogeological investigation in support of two Draft Plan of Subdivision applications. The Badenview and New HamburgIrs properties are referred to herein as the 'Subject Lands'. For the purposes of this report the two draft plans will be reviewed as one cohesive development. The Subject Lands are located within what is commonly referred to as the Wilmot Employment Lands (WEL) in the Town of New Hamburg, Township of Wilmot.

The WEL comprise of two parcels of land, formerly known as the Good Lands and the Schneider Lands. The Good Lands are owned by Badenview Developments Inc. The Schneider Lands are owned by New HamburgIrs Inc. Refer to **Figure 1a** for the Subject Lands Location Map and **Figure 1b** for the Subject Lands Key Map.

The proposed development includes industrial lands, municipal roadways and a Stormwater Management (SWM) Facility, which is currently being proposed to be located within the south portion of the Good Lands. The Subject Lands are to be serviced with municipal water and storm and sanitary sewers.

Note: The Ontario Ministry of the Environment, Conservation and Parks (MECP) was previously named the Ontario Ministry of the Environment (MOE) and the Ontario Ministry of the Environment and Climate Change (MOECC). For ease of discussion in this report, "MECP" is used to represent this provincial ministry and is inclusive of MOE and MOECC.

1.2 Scope and Methodology

The objective of this study is to investigate the potential impacts associated with the proposed development on the Subject Lands. More specifically, this investigation will:

- Assess the local and regional hydrogeological characteristics;
- Determine local groundwater elevations and interpret flow direction;
- Determine infiltration opportunities; and
- Provide a preliminary assessment for the need for construction dewatering.

To meet the objective, the following scope of work was implemented:

- 1) Site Identification:
 - Legal description.
 - Site Features.
 - Neighbouring land uses.
 - Ministry of the Environment, Conservation and Parks (MECP) well records review.
 - Published map review:

- Ontario Base Maps;
- Quaternary geology maps; and
- Bedrock geology maps.
- Review of the Township of Wilmot and the Regional Municipality of Waterloo Official Plans.
- Review of existing geology and hydrogeological reports.
- Review of interactive online mapping tools:
 - Grand River Conservation Authority (GRCA) Source Water Protection Plan; and
 - GRCA Regulation Areas.
- 2) Field Investigation:
 - Review of select off-site wells within 1000 m of the Site to identify:
 - Neighbouring wells;
 - o Well depths;
 - o Well construction details; and
 - Local geological information.
 - Installation of 11 overburden groundwater monitoring wells on-site.
 - In-situ hydraulic response testing of 11 on-site groundwater monitoring wells to determine hydraulic conductivity.
- 3) Analysis and Reporting:
 - Geologic and hydrogeological summary.
 - Preparation of geological cross-sections through the Subject Lands.
 - Assessment of potential hydrogeological impacts from the proposed development on the Subject Lands.
 - Determination of shallow groundwater system properties:
 - Horizontal hydraulic gradient;
 - Average linear groundwater velocity; and
 - o Shallow groundwater flow patterns.
 - Assess stormwater management measures proposed with respect to quantity of groundwater inputs to local aquifers.

This report should be read in conjunction with the following reports that have also been completed by MTE for the Subject Lands:

- Functional Servicing Report, dated December 17, 2018
- Preliminary SWM Report, dated December 17, 2018
- Preliminary Grading and Cut/Fill Analysis, dated December 17, 2018

1.3 **Previous Studies**

MTE reviewed a number of reports and documents applicable to the Subject Lands regarding the physical framework and hydrogeological characteristics, some regional in nature and some Site specific. Previous works completed and reviewed for the purposes of this study include:

 Enhanced Master Drainage Plan – Wilmot Employment Lands, New Hamburg, ON, last revised May 22, 2012, (MTE); and • Preliminary Engineering Design and Cost Analysis – Wilmot Employment Lands, Township of Wilmot, July 2004 (Stantec).

A Geotechnical Investigation Report was completed for the Wilmot Employment Lands by Peto MacCallum Ltd. (Peto), dated December 18, 2018. A Geotechnical Investigation Report was completed for the Highway 7 & 8 New Hamburg Lands by Peto, dated December 18, 2018.

2.0 SUBJECT LANDS DESCRIPTION

The Subject Lands comprise a total area of approximately 55.38 hectares. The legal description of the Good Lands is:

Part of Lots 19-21, Concession North, Bleams Road Part of Lot 21 Concession South, Bleams Road Township of Wilmot Regional Municipality of Waterloo

The legal description of the Schneider Lands is:

Part of Lot 19, South Snyder's Road Part of Lot 19 North of Bleams Road North of Highway 7 & 8 Township of Wilmot Regional Municipality of Waterloo

The Study Area for the Subject Lands, including the boundary, geological cross-section locations, monitoring wells and existing features is illustrated on **Figure 2** and **Figure 3**.

Land use within the Subject Lands is primarily agricultural. The Township of Wilmot Official Plan identifies an area of Environmentally Constrained Lands within the south portion of the Subject Lands. This feature is associated with the presence of a floodplain as identified through the GRCA online mapping tool and shown on **Figure 3**.

A Draft Plan of Subdivision for the proposed Good Lands development has been prepared by MHBC Ltd., dated November 22, 2018. The Draft Plan of Subdivision includes industrial blocks, a Stormwater Management Facility block, road widenings, future development blocks, 0.3m reserve blocks and municipal roadways comprising a total area of approximately 42 hectares. The Draft Plan of Subdivision for the Good Lands is enclosed in **Appendix A**.

A Draft Plan of Subdivision for the proposed Schneider Lands development has been prepared by MHBC Ltd., dated November 22, 2018. The Draft Plan of Subdivision includes industrial blocks, emergency access blocks and municipal roadways comprising a total area of approximately 10 hectares. The Draft Plan of Subdivision for the Schneider Lands is enclosed in **Appendix A**.

2.1 Adjacent Land Use

The Subject Lands are bounded by industrial lands to the east and north, Highway 7/8 to the south and existing residential and industrial properties to the west. A woodlot and existing CN/GEXR railway line is present to the north. The Township of Wilmot Official Plan classifies the woodlot as a Locally Significant Natural Area (Map No. 8). In addition, a GRCA-defined wetland is located approximately 30m west of the Subject Lands. The Region of Waterloo Official Plan identifies this feature as a Core Environmental Feature.

2.2 Topography and Surface Water Drainage

MTE conducted a detailed topographical survey in 2018. A topographical low is located within the southeast portion of the Good Lands. The Subject Lands are moderately sloped throughout the majority of the site (generally between 1% and 10%). Existing elevations range between 346.6m at the centerline of Hamilton Road, 346.3 metres above mean sea level (mamsl) at the centerline of Nafziger Road, 346.0mamsl at the highest point of the GEXR, down to 334.2mamsl at the lowest point at the southern property line near an existing drainage outlet.

Overland surface water runoff follows topography towards the topographic low in the southeast corner of the Good Lands.

The Subject Lands currently contain two drainage outlets, known as the east and west tributaries, located near the southeast border of the Good and Schneider Lands and the southwest corner of the Good Lands, respectively, as illustrated on **Figure 4**. Both of these tributaries drain to the Nith River. The area of the Subject Lands that are classified as a floodplain by the GRCA and Environmentally Constrained Lands by the Township of Wilmot is located upstream of the west tributary.

An extensive network of tile drainage is present beneath the Good Lands (**Figure 4**), which outlet immediately upstream of the western tributary. Based on discussions with persons knowledgeable about the Subject Lands, there may be tile drainage beneath the Schneider Lands. If present, the network is no longer in service. No tile drains were encountered within the Schneider Lands during borehole advancement or test trench excavation.

According to the Grand River Information Network (GRIN) online mapping tool, a GRCA-defined wetland is located approximately 30m north of the WEL. There are no provincially significant wetlands located within or adjacent to the Subject Lands.

The Subject Lands are located within the Nith River Subwatershed in the Township of Wilmot. The Nith River (located approximately 870m south and 790m west of the Subject Lands) drains into the Grand River.

2.3 Development Proposal

Development as Proposed by Draft Plan

As illustrated on the proposed Draft Plan of Subdivisions, the proposed developments are made up of a number of blocks comprising industrial blocks, a stormwater management facility, municipal right-of-ways, and MTO setbacks areas.

Municipal Servicing

The proposed development will be serviced by municipal water, sanitary sewer and storm sewers. The reader is referred to the Wilmot Employment Lands Industrial Subdivision, Functional Servicing Report completed by MTE, dated December 17, 2018 for information relating to the proposed municipal servicing within the Subject Lands.

Stormwater Management (SWM)

The proposed development includes a SWM facility in the south portion of the Good Lands. The reader is referred to the Wilmot Employment Lands Industrial Subdivision, Stormwater Management Report completed by MTE, dated December 17, 2018 for information relating to the proposed SWM facility within the Subject Lands.

3.0 FIELD PROGRAM

3.1 Borehole Advancement and Monitoring Well Installation

The 2011 hydrogeological assessment completed for the Enhanced Master Drainage Plan (MTE, 2011) included the advancement of 12 boreholes (BH1-11 through BH12-11) to depths ranging between 8.2 metres below ground surface (mbgs) to 9.1mbgs, 11 test trenches (TT1-11 through TT11-11) to depths of 3.3mbgs, and three minipiezometers (MP1-11 through MP3-11) to depths ranging between 0.91mbgs to 1.22mbgs on or within the area surrounding the Subject Lands. No monitoring wells were installed as part of the 2011 assessment.

A total of 11 boreholes (BH101-18 through BH109-18, BH111-18 and BH115-18) were advanced at the Good Lands between March 12 and 26, 2018 as part of a geotechnical investigation completed by Peto. Boreholes were advanced to depths ranging from 3.6mbgs to 11.1mbgs and were observed by Peto. Seven of these boreholes were completed as groundwater monitoring wells (BH101-18 through BH107-18). In addition, two mini-piezometers (MP2-11 and MP3-11) were replaced by MTE as these were found to be damaged. The MP2-11 and MP3-11 replacements were installed to depths of 0.93m and 0.98mbgs, respectively.

A total of six boreholes (BH201-18 through BH206-18) were advanced at the Schneider Lands on June 6, 2018 as part of a geotechnical investigation completed by Peto. Boreholes were advanced to a depth of 6.7mbgs and were observed by Peto. Four of these boreholes were completed as groundwater monitoring wells (BH201-18 through BH204-18).

Five test trenches were advanced at the Good Lands on July 20, 2018 (TT1-18 through TT5-18). An additional five test trenches were advanced at the Schneider Lands on October 25, 2018 (TT6-18 through TT10-18). Test trenches were completed by Musselman Excavating and were observed by MTE. Test trenches were advanced to depths ranging from 4.1mbgs to 6.4mbgs which was based on field observations of geologic conditions in order to meet the project objective.

All borehole, monitoring well, test trench, and mini-piezometer locations are illustrated on **Figure 3**. Borehole logs are provided in **Appendix B**.

Following installation, monitoring wells were developed using Waterra[™] Surge Blocks to remove any accumulated silt and sediments from the bottom of the well and to remove fine materials from the well screen and sand pack.

Soil conditions observed during borehole and test trench advancement at the Subject Lands generally consist of topsoil ranging in thickness from 0.05m to1.2m underlain by native clayey silt, and silt material to the maximum investigated depth of 11.1mbgs. Occurrences of sandy silt were observed at borehole locations BH103-18 and BH105-18 while occurrences of silty sand were observed at borehole locations BH104-18, BH109-18 and BH202-18. These observations are characteristic of the Maryhill Till geological unit.

Bedrock was not encountered in any of the boreholes advanced on the Subject Lands; however, it is anticipated to be approximately 31 to 64mbgs (refer to Section 4.3).

3.2 Water Well Record Search

Hydrogeological data related to private supply wells within 1000m of the Subject Lands were obtained from water well records on-file with MECP. A total of 34 water well records were located within 1000m of the Subject Lands, as shown on **Figure 2**. Of the 34 water well records:

- Two wells were listed as commercial wells (ID No.'s 6506377 & 6508207);
- Eighteen wells were listed as domestic/livestock use wells, two of which are located on the Subject Lands (ID No.'s 7053495 & 6509204);
- Three wells were listed as industrial wells;
- Six wells were listed as monitoring wells/monitoring and test holes/test holes; and
- Five wells were listed as "not used".

There were no wells identified as municipal water supply wells.

Based on data obtained from the available well records, overburden in the area is generally comprised of silt and clay with various quantities of sand and stones reported.

MECP well records are available online within the MECP Well Records database.

3.3 Groundwater Levels

MTE completed twelve rounds of manual groundwater level measurements between April 8, 2018 and October 12, 2018. Manually measured groundwater levels and elevations within the monitoring wells are presented in Table 1 and Table 2.

Manual water level measurements were also collected from the three mini-piezometers in order to assess the vertical gradients from the wetland to the shallow groundwater system. Table 3 presents the manually measured water levels, elevations and vertical hydraulic gradient calculations within the mini-piezometers.

Electronic pressure transducers (data loggers) were installed within each of the monitoring wells within the Good Lands on June 1, 2018 and within the Schneider Lands on August 10, 2018. Data loggers measure the pressure (in centimeters of water) above the logger at a predetermined time interval, which can then be used to calculate a groundwater level and elevation. The data loggers installed at the Subject Lands were set to record a pressure at a time interval of every 1 hour. Hydrographs illustrating continuous groundwater elevations within the monitoring wells at the Subject Lands are provided in **Appendix C**. Based on the data logger recorded measurements, groundwater elevations were measured to range between 331.74mamsl (BH103-18) and 340.12mamsl (BH105-18).

Daily precipitation data was plotted on the hydrographs to determine how the water table responds to precipitation events. The precipitation data was obtained from the Government of Canada website as reported from the Kitchener/Waterloo weather station (operated by NAVCAN) located at the Region of Waterloo International Airport.

As shown on the hydrographs, monitoring well locations BH101-18 through BH105-18, BH107-18, BH201-18 and BH204-18, show responses to precipitation events however; these responses appear delayed which is likely attributed to the fine-grained soil material and associated low infiltration and percolation rates. Responses to precipitation events were not apparent at monitoring locations BH106-18, BH202-18 and BH203-18 which is likely a result of the heterogeneity of the soils beneath the Subject Lands.

Groundwater levels at the Subject Lands are likely subject to seasonal fluctuations, with seasonal highs expected in the early spring during snow melt. Continuous monitoring of groundwater elevation data will allow for the assessment of seasonal fluctuations of the water table and provide additional information on the short-term responses to precipitation events.

3.4 Hydraulic Conductivity Testing

Qualitatively, hydraulic conductivity (K) is a parameter describing the ease with which groundwater flows through a porous medium. Relatively large K values are attributed to permeable units, i.e. sand and gravel, while small values are attributed to less permeable material (i.e. silt or clay). Representative K values for various soil types are presented in Freeze and Cherry (1979).

MTE conducted single well hydraulic response tests on select on-Site monitoring wells on April 13, 2018 and October 10, 2018 in order to estimate the hydraulic conductivity of the screened interval beneath the Subject Lands. A recovery test (i.e. rising head test) was selected as the testing method due to the expected slow recoveries observed during well development. Recovery testing included purging the well dry, after development with a surge block, and using a pressure transducer (data logger) to record the pressure (in centimeters of water) above the logger during recovery. This pressure was then used to calculate a groundwater level. The data logger was programmed to record a reading every 10 or 60 seconds, in order to adequately capture the well recovery.

Prior to conducting the slug test analysis, recovery data was normalized by dividing the measured drawdown by the maximum recorded drawdown. Water level response data was analyzed using the Hvorslev method (Fetter, 2001) as, upon comparison with the Bouwer and Rice method (Fetter, 2001), more conservative values were calculated.

4.0 REGIONAL HYDROGEOLOGICAL SETTING

4.1 Physiography

The Subject Lands are located in the physiographic region known as the undrumlinized Stratford Till Plain, which consists of a broad clay plain extending from London in the south to Blyth and Listowel in the north. The till is fairly uniform and consists of brown, calcareous silty clay. Sand or gravel is often present in the intermorainal valleys south of St. Mary's (Chapman and Putnam, 1984). **Figures 5a** and **Figure 5b** show the location of the Subject Lands in relation to the physiographic regions and landforms, respectively.

4.2 Quaternary Geology

The Region of Waterloo has relatively thick glacial overburden deposits overlying bedrock attaining thicknesses in excess of 100m. In general, silty to clayey till was deposited as extensive sheets during different periods of glacial ice advance. Granular materials, such as outwash and kame sand, gravels and glaciolacustrine fine-grained deposits (such as silt and clay), were deposited during the ice retreat (Karrow, 1993).

The Quaternary Geology Map (**Figure 6**) identifies regional surficial deposits of clay to silt-textured till with pockets of ice-contact stratified deposits of sand and gravel with minor silt, clay and till.

4.3 Paleozoic Geology

The Region of Waterloo (ROW) is underlain, east to west and oldest to youngest, by Silurian age Guelph (dolostone), Salina (dolostone, shale, salt and gypsum) and Bass Islands (dolostone) Formations. Directly beneath the Subject Lands lies the Salina Formation (Hewitt, 1972), as shown on **Figure 7**.

Bedrock was not encountered during the drilling program, however according to the depth to bedrock reported in MECP well records in the area and borehole logs provided by the ROW, it is anticipated bedrock will be encountered at approximately 31mbgs to 64mbgs.

4.4 Regional Hydrogeology Setting

The ROW obtains approximately 80% of its water supply from groundwater within bedrock and sedimentary aquifers, with approximately half being supplied from the Waterloo Moraine (Bajc et. al., 2014). The Waterloo Moraine is located almost entirely within the ROW and is comprised of three separate units, which grade from coarse-grained sediments (gravel) to finer-grained sediments (silt and clay) with decreasing depth (Bajc et. al., 2014).

The fine-grained units of the Waterloo Moraine are referred to as the Upper, Middle, and Lower Maryhill Tills. These units represent regionally significant aquitards and will "act as a significant barrier to vertical water movement where present in a thickness greater than 5 meters" (Terraqua Ltd., 1995). The Maryhill Till consists primarily of sandy silt to silty clay and clayey silt diamictons (Bajc et. al., 2014). The Waterloo Moraine Aquifer Units are characterized by interbedded layers of silt, sand and gravels. Clay-rich glaciolacustrine deposits with gravels and pebbles are also present.

These Waterloo Moraine sediments overlie the Catfish Creek Till, characterized as a stoney to sandy diamicton, which is often over consolidated and forms an important marker horizon within the Region of Waterloo (Karrow, 1987). The Catfish Creek Till acts as an important, relatively continuous regional aquitard that is compositionally distinct and is widely distributed across the ROW (Terraqua Ltd., 1995; Bajc and Shirota, 2007; AquaResource Inc., 2009).

Regional groundwater elevations, provided from the GRIN, indicate that the regional groundwater flow direction in the area surrounding the Subject Lands is westerly, towards the Nith River (**Figure 8**).

5.0 LOCAL HYDROGEOLOGICAL SETTING

Previously drilled boreholes, MECP water well records and current boreholes and monitoring wells installed in 2018 were used to interpret local hydrostratigraphic units and generate four geological cross-sections.

Regional Geological Cross-Sections (Cross-Section A-A' and B-B') are presented on **Figure 9** and **Figure 10**, respectively. Local Geological Cross-Sections (Cross-Section C-C' and D-D') are presented on **Figure 11** and **Figure 12**, respectively. The cross-section stratigraphy was drawn using HydroGeo Analyst (HGA), which is a relational database system used to store and query the project database to create cross-sections.

Regional Geological Cross-Sections

Geological Cross-section A-A' (Figure 9):

- Extends approximately 3.0km north to south through the Subject Lands;
- Illustrates undulating topography from north to south with a large depression at the southern-most extent as the Nith River is approached;
- Portrays a subsurface comprised of overburden aquitard material (ATB1/ ATB3) composed primarily of fine-grained sediment (clayey silt to silty clay Maryhill Till) ranging in thickness from approximately 25m to 38m;
- Illustrates a relatively small, localized lens of silty sand within the central area of the property extending to the south which is bounded above and below by finergrained sediments (Maryhill Till);
- Illustrates a fine-grained unit with a higher content of coarse-materials (i.e. gravel) extending across the entire section at elevations between approximately 323mamsl to 329mamsl which gradually increases in thickness towards the south; and
- Infers the shallow groundwater table is located at elevations ranging between approximately 335m amsl to 338m amsl, based on the October 12, 2018 groundwater measurements, generally decreasing towards the south.

Geological Cross-section B-B' (Figure 10):

- Extends approximately 2.6km west to east through the southern portion of the Subject Lands;
- Illustrates the Nith River and respective basin to the west, representing the topographic low, followed to the east by gently undulating topography with the Subject Lands crossing a topographical depression;
- Portrays overburden material in the Study Area to be comprised of fine-grained sediment deposits of clayey silt/silty clay till material characteristic of the Maryhill Till geological unit, ranging in thickness from approximately 20.5m (beneath the bed of the Nith River) to 41.5m;

- Illustrates a relatively small, localized lens of silty sand at an elevation of approximately 336m amsl and a fine-grained layer with a higher content of coarse materials (gravel) at an elevation of approximately 327m amsl within the center of the Subject Lands at the intersection of Cross-Section A-A. The lateral extent of these units from east to west is unknown; and
- Does not indicate an inferred groundwater table elevation as there was insufficient information; however, one location within the limits of the Subject Lands illustrates a groundwater elevation of 339.7m amsl.

Local Geological Cross-Sections

Geological Cross-section C-C' (Figure 11):

- Extends approximately 855m west to east through the south portion of the Subject Lands;
- Shows overburden material at the Subject Lands consists of fine-grained sediment deposits of clayey silt/silty clay till, characteristic of the Maryhill Till geological unit, from ground surface to the depth explored; and
- Illustrates the shallow groundwater table in the south portion of the Subject Lands ranges between approximately 335m amsl to 339.2m amsl. It is noted that that groundwater table is above the ground surface at BH103-18.

Geological Cross-section D-D' (Figure 12):

- Extends approximately 782m north to south through the east portion of the Subject Lands (Schneider Lands);
- Shows overburden material at the Subject Lands consists of fine-grained sediment deposits of clayey silt/silty clay till, characteristic of the Maryhill Till geological unit, from ground surface to the depth explored;
- Illustrates a seam of coarser-grained silty sand material in approximately the center of the section at BH202-18, which was identified at approximately 335mamsl and extended to the depth explored at BH202-18. Therefore; the width of this unit is currently unknown; and
- Illustrates the shallow groundwater table beneath the east portion of the Subject Lands ranges between approximately 336.9m amsl to 339.8m amsl.

5.1 Hydraulic Conductivity

The single well hydraulic response test analysis resulted in K values ranging from 2.0 $\times 10^{-8}$ m/sec to 1.6 $\times 10^{-6}$ m/sec with a geometric mean of 9.8 $\times 10^{-8}$ m/sec. These results are consistent with the average published values for silt and glacial till soils (Freeze and Cherry, 1979) and the calculated K estimates from the geotechnical investigation, which reported a K value of "less than 1x10⁻⁸m/sec" for the clayey silt material and 1x10⁻⁶m/sec for the Silt, Sandy Silt and Silty Sand material.

Table 5.1 below summarizes the hydraulic conductivity estimates for each analyzed data set. **Appendix D** provides AquiferTest Pro data sheets.

Location	K value (m/sec)
BH101-18	4.6x10 ⁻⁸
BH102-18	3.9x10 ⁻⁸
BH104-18	3.9x10 ⁻⁸
BH105-18	4.0x10 ⁻⁷
BH106-18	1.6x10 ⁻⁶
BH107-18	4.0x10 ⁻⁸
BH201-18	2.0x10 ⁻⁸
BH202-18	1.1x10 ⁻⁷
BH204-18	2.2x10 ⁻⁷
Minimum	2.0x10 ⁻⁸
Maximum	1.6x10 ⁻⁶
Geo-Mean	9.8x10 ⁻⁸

 Table 5.1: Hydraulic Conductivity (K) Values (m/sec)

5.2 Groundwater Flow and Average Linear Groundwater Velocity

The interpreted groundwater flow direction was determined using the October 12, 2018 groundwater elevation data. **Figure 13** illustrates groundwater elevation contours and flow patterns, indicating that the local groundwater system beneath the Subject Lands generally flows towards a hydraulic low located within the south portion of the Good Lands. Groundwater flow in the north portion of the Good Lands appears to flow in a northerly direction. The inconsistency between the regional groundwater flow direction interpretation (westerly) and the inferred groundwater flow direction within the west portion of the Good Lands may be due to the influence of the tile drainage network beneath the Subject Lands (**Figure 4**), and the influence of the local topography within the Site.

The horizontal hydraulic gradient is a measurement of the slope of the water table surface which is simply the change in hydraulic head over the change in distance between two or more monitoring points. **Figure 13** was used to calculate the horizontal hydraulic gradient which was estimated to be approximately 0.01m/m.

The average linear groundwater velocity was estimated based on three variables: hydraulic conductivity, horizontal hydraulic gradient and effective soil porosity. Effective soil porosity (n_e) is the percentage of a soils total porosity that allows for fluid flow through the soil (Fetter, 2001).

The equation for calculating average linear groundwater velocity is:

 $v = (-Ki)/n_e$ [Eq. 1.]

Where:

v = average linear groundwater velocity (m/sec) K = hydraulic conductivity (9.8x10⁻⁸m/sec (geometric mean)) i = horizontal hydraulic gradient (dh/dl) (0.01m/m) n_e= effective soil porosity (0.25 typical for a silty clay (Bonazountas and Wagner, 1981))

With respect to the above values, the average linear groundwater velocity (v) within the shallow groundwater system at the Subject Lands was estimated to be approximately 0.12 m/year.

5.3 Groundwater – Wetland Interaction

Vertical hydraulic gradients were calculated to provide insight into whether the wetland was gaining (i.e. receiving groundwater from below) or losing (i.e. recharging the shallow groundwater table through infiltration).

Vertical hydraulic gradients were calculated using the following equation:

G = (OL - IL) / (MD - OL - [0.5 x L]) [Eq.2.]

Where:

G = hydraulic gradient (m/m) OL = outside water level at MP (measured from top of MP casing) (m) IL = inside water level at MP (measured from top of MP casing) (m) MD = measured depth of MP (measured from top of MP casing) (m) L = screen length (m)

 Table 3 summarizes the calculated vertical gradients from the three MPs.

Where measureable, the vertical hydraulic gradient within the wetland at the three minipiezometers was negligible representing relatively stagnant water conditions. Vertical hydraulic gradients can vary throughout the year and are influenced by precipitation events.

Determining the interaction between the groundwater and wetland located northwest of the Subject Lands included comparing the average and maximum groundwater elevations recorded in proximity to the wetland (at monitoring location BH107-18) to the average and minimum water elevations recorded inside the mini-piezometers (MP1-11 through MP3-11). The results of this comparison found that the difference between the water levels was, on average, approximately 2.45m, with the minimum separation measured as 0.14m (measured at MP1-11 on June 1, 2018). In addition, two of the mini-piezometers were observed to have "dry" outside levels during this investigation (MP1-11 and MP2-11). Hydrograph 12 in Appendix C illustrates the continuous water level measurements as recorded in MP3-11. As shown, the water level within MP3-11 responds to precipitation events, and the water level within the mini-piezometer gradually decreases during periods of low precipitation.

Based on the separation distances and observed "dry" conditions at two of the minipiezometers, and the trends observed from the continuous water level monitoring within MP3-11, is interpreted that the wetland is not maintained by groundwater discharge.

The wetland likely receives water inputs as sheet runoff and from small independent subcatchment areas. When water inputs occur, overflows would rise above the organic seal of the wetland beds and, due to the low permeability soils at ground surface, surface water runoff from the wetland would result. Additional losses occur through evapotranspiration which can cause some wetlands to either dry up or experience a receding of their limits within the summer months, and is dependent on the amounts of precipitation.

The soils underlying the wetland were found to consist of clayey silt with similar characteristics to that found throughout the Subject Lands. Therefore, it is expected that surface water infiltration beneath the wetland is very slow.

6.0 SOURCE WATER PROTECTION

6.1 Wellhead Protection Areas

Based on the MECP on-line interactive Source Water Protection Information Atlas (MECP, 2018), no portion of the Subject Lands fall within a Wellhead Protection Area (WHPA), as shown on **Figure 14**.

6.2 Intrinsic Vulnerability

MTE reviewed the GRIN for information pertaining to the aquifer Intrinsic Vulnerability. The Intrinsic Vulnerability of an aquifer is based on the nature of the soil and/or bedrock and how easily surface water can reach the aquifer. Intrinsic Vulnerability is ranked as low, medium or high and does not take into consideration the properties of the contaminant itself (Liggett, Lapcevic, & Miller, May 2011).

As shown on **Figure 15**, the majority of the Subject Lands are classified as Medium Intrinsic Vulnerability with the exception of an area in the northeast portion of the Good Lands which is classified as Low Intrinsic Vulnerability.

6.3 Municipal Well Fields

The closest municipal well field is the New Hamburg Well Field, located approximately 2.25 km southwest of the Subject Lands housing one supply well (NH03). The well is screened from approximately 57mbgs to 76mbgs within the bedrock aquifer (LESPC, 2015).

Based on the distance to the closest municipal well field and the well screened depth, the proposed development is not anticipated to impact municipal water supply.

6.4 Significant Groundwater Recharge Areas (SGRAs)

Groundwater recharge occurs where precipitation and snowmelt infiltrate into the ground to feed aquifers, watercourses and wetlands. SGRAs are typically associated with coarse-grained soils (i.e. sands and gravels) or very shallow overburden material covering upland areas on the landscape. The GRIN shows that no portion of the Subject Lands is within a SGRA.

6.5 Issue Contributing Areas (ICAs)

ICAs were developed to define areas where past or current activities have or are likely to adversely affect the quality of drinking water in a given municipal well in which contaminants have already been measured at elevated levels.

An ICA is defined by the Grand River Source Protection Plan as:

"The area within which activities have or are likely to contribute to the elevated contaminant at the well...in most cases, an ICA is the 25 year time-of-travel capture zone." (Grand River Conservation Authority, 2015)

The GRCA GRIN on-line map shows that no portion of the Subject Lands is within an ICA.

7.0 IMPACT ASSESSMENT

7.1 Stormwater Infiltration Design Considerations

Background evaluation and local field testing conducted under this hydrogeological investigation determined the Subject Lands were unsuitable for infiltration testing due to the fine-grained material, characteristic of the Maryhill Till geological unit, which does not readily transmit water, present throughout the majority of the Subject Lands.

A calculated infiltration rate was provided by Peto as "less than 0.04mm/hr" for clayey silt materials and 5mm/hr for silt, sandy silt, and silty sand material. As a result, the amount of infiltration is considered "negligible". This is consistent with the presence of a thick aquitard unit beneath the ground surface.

Soil samples collected from test trench locations TT1-18 and TT5-18 were submitted to Peto for particle size distribution analysis and an estimate of hydraulic conductivities and infiltration rates. TT1-18 is located within the footprint of the proposed SWM facility. The sample submitted from TT1-18 was collected from a depth of 4mbgs and was characterized as a silt with an estimated hydraulic conductivity of 1×10^{-6} m/sec and infiltration rate of 10mm/hour. The sample submitted from TT5-18 was collected from a depth of 4mbgs and was characterized as a clayey silt with an estimated hydraulic conductivity of 1×10^{-6} m/sec and infiltration rate of 1×10^{-8} m/sec and 1×10^{-8} m/sec and 1×10^{-8} m/sec and 1

The geotechnical grain size analysis report outlining the results from the test pitting program is provided in **Appendix E**.

7.2 Groundwater Separation to Grade at SWM Pond

Based on the proposed Draft Plan of Subdivision for the Good Lands, three groundwater monitoring locations are located within the limits of the proposed SWM facility: BH101-18 to BH103-18. The maximum groundwater elevations measured at these locations throughout this investigation are provided in **Table 7.2.1**, below:

Location	Maximum Water Table Elevation (mamsl)
BH101-18	337.54
BH102-19	335.29
BH103-18*	334.65

*The groundwater elevation at BH103-18 represents an above-ground elevation.

These elevations will need to be taken into consideration upon finalizing the design of the SWM facility. In addition, construction dewatering may be required.

7.3 Groundwater Separation and Site Grading

Composite high groundwater table elevations for the Subject Lands are provided on **Figure 16**. The composite high water level map is a conservative representation of the seasonal high water levels during the spring freshet period (i.e. wet period) and is used to determine if adequate separation exists between the proposed floor foundation elevation and the shallow water table condition.

Although the proposed design specifications for the industrial buildings were unknown at the time of writing this report the development can still be constructed in this low permeable environment with adequate engineering design to move water away from the building foundations (e.g. installing a weeping tile system that collects water pumped out of a designated sump pump system). The potential long-term shallow groundwater flux into the designated sump pump system(s) is expected to be negligible considering that the subsurface soil material is low permeability (i.e. 10^{-8} m/sec). It is anticipated that sump pumps will only being active for short period of time, mainly during the spring freshet periods when the water levels are high.

7.4 Servicing Considerations

The Subject Lands will be serviced by municipal water, sanitary sewers and storm sewers. Refer to the Wilmot Employment Lands Industrial Subdivision, Functional Servicing Report completed by MTE for information relating to the proposed municipal servicing within the Subject Lands.

Composite high groundwater table elevations for the Subject Lands are provided on Figure 16.

Based on the composite high groundwater table elevation contours, the groundwater table may be encountered during the spring freshet periods only. Therefore, depending on when the installation of these services is constructed, a dewatering assessment may be required. The use of cut-off collars is recommended in these areas to prevent the migration of groundwater through pipe bedding and backfill. If the water table is encountered, the volumes produced may not exceed 50,000 L/day and therefore a Permit to take Water (PTTW) or Environmental Activity Sector Registry (EASR) may not be required. MTE does not anticipate managing large volumes of discharge water based on the low permeable subsurface soil environment.

7.5 Wetland Assessment

As outlined in Section 5.3, it is interpreted that the wetland located north of the Subject Lands is not maintained by groundwater discharge. Therefore, dewatering activities within the Subject Lands, if required, is not anticipated to impact the wetland.

Surface water runoff, post-construction, is anticipated to be directed towards the proposed SWM facility, located within the south portion of the Good Lands. Therefore, the development is not likely to impact the wetland as the wetland is located up-gradient within the property and therefore will not receive additional surface water inputs post-development.

8.0 SUMMARY AND CONCLUSIONS

Based on this hydrogeological investigation, MTE offers the following findings:

<u>Geology</u>

- Stratigraphic conditions beneath the Subject Lands primarily consist of finegrained (clayey silt, silt, silt till, etc.) materials characteristic of the Maryhill Till geological unit; and
- Bedrock is anticipated to be at approximately 31 to 64mbgs.

<u>Hydrogeology</u>

- The shallow groundwater table was encountered at a depth range of 0.92m above the ground surface at BH103-18 to 6.61mbgs, at elevations between 327.0mamsl to 340.2mamsl during this investigation;
- The regional groundwater flow is inferred to be westerly, towards the Nith River, while the local groundwater flow direction is inferred to be towards a hydraulic low located within the south portion of the Good Lands. Groundwater flow in the north portion of the Good Lands is inferred to be northerly;
- The expansive network of tile drainage beneath the Subject Lands may be influencing the local shallow groundwater table;
- The horizontal hydraulic gradient is estimated to be 0.01 m/m;
- Hydraulic conductivity values ranged between 2.0 x10⁻⁸ m/s to 1.6 x10⁻⁶ m/s with a geometric mean of 9.8 x10⁻⁸ m/s; and
- The groundwater velocity of the shallow groundwater table beneath the Subject Lands was estimated to be 0.12 m/year.

Impact Assessment and Construction Considerations

Proposed SWM Facility

- The sample submitted from TT1-18 (located within the proposed SWM facility block) from 4mbgs and was characterized as a silt with an estimated hydraulic conductivity of 1x10-6m/sec and infiltration rate of 10mm/hour; and
- Construction dewatering may be required.

Groundwater Separation and Site Grading

• Although the proposed design specifications for the industrial buildings were unknown at the time of writing this report the development can still be constructed in this low permeable environment with adequate engineering design in order to move water away from the building foundations (e.g. installing a weeping tile system that collects water pumped out of a designated sump pump system). It is anticipated that sump pumps will only being active for short periods of time (i.e. spring freshet periods when the water levels are high).

Servicing Considerations

- The groundwater table may be encountered during the installation of services and construction dewatering may be required. The use of cut-off collars is recommended in these areas to prevent the migration of groundwater through pipe bedding and backfill; and
- If the water table is encountered during construction, the volumes produced may not exceed 50,000 L/day and therefore a Permit to take Water (PTTW) or Environmental Activity Sector Registry (EASR) may not be required.

8.1 Recommendations and Monitoring

MTE recommends the Draft Plan Conditions require the following:

- Continuous groundwater monitoring;
- Updated information should be utilized during final design of the development as well as during the design of the site plan blocks;
- Mini-piezometers MP1-11 through MP3-11 should be monitored on continuous basis, during ice-free months, for a minimum period of one year, as outlined in the Work Program dated December 22, 2017;
- Further assessment of the requirement for construction dewatering, including whether a PTTW or EASR is required;
- During the development application process, existing on-site groundwater monitoring wells be maintained in accordance with Ontario Regulation 903 (as amended); and
- Prior to construction activities, monitoring wells located within proposed construction areas will need to be decommissioned in accordance with Ontario Regulation 903 (as amended).

9.0 LIMITATIONS

Services performed by **MTE Consultants Inc.** (MTE) were conducted in a manner consistent with the level of care and skill ordinarily exercised by members of the Environmental Engineering & Consulting profession. No other warranty or representation expressed or implied as to the accuracy of the information, conclusions or recommendations is included or intended in this report.

This report was completed for the sole use of MTE and the Client. The assignment was carried out in accordance with the Scope of Work described in Section 1.1 as reviewed with and agreed to by the Client. MTE makes no representation that the present report has dealt with all of the important environmental issues, except as provided in the Scope of Work. This report is not intended to be exhaustive in scope or to imply a risk-free facility. As such, this report may not deal with <u>all</u> issues potentially applicable to the Site and may omit aspects which are or may be of interest to the reader.

In addition, it should be recognized that a soil sample or groundwater level measurement represents one discrete portion of the Site at the time it is collected, and that the findings of this report are based on conditions as they existed during the time period of the investigation.

Any use which another party makes of this report, or any reliance on, or decisions to be made based upon it, are the responsibility of such parties. MTE accepts no responsibility for liabilities incurred by or damages, if any, suffered by another party as a result of decisions made or actions taken, based upon this report. Others with interest in the Site should undertake their own investigations and studies to determine how or if the condition affects them or their plans.

It should be recognized that the passage of time may affect the views, conclusions and recommendations (if any) provided in this report because environmental conditions of a property can change, along with regulatory requirements. Should additional or new information become available, MTE recommends that it be brought to our attention in order that we may determine whether it affects the contents of this report.

Respectfully Submitted,

MTE CONSULTANTS INC.

Kassandra Wallace, B.B.R.M. Environmental Scientist

KLW:dem

PRACTISING MEMBE

Robert Maric, M.Sc., P.Geo., QP_{ESA} Hydrogeologist

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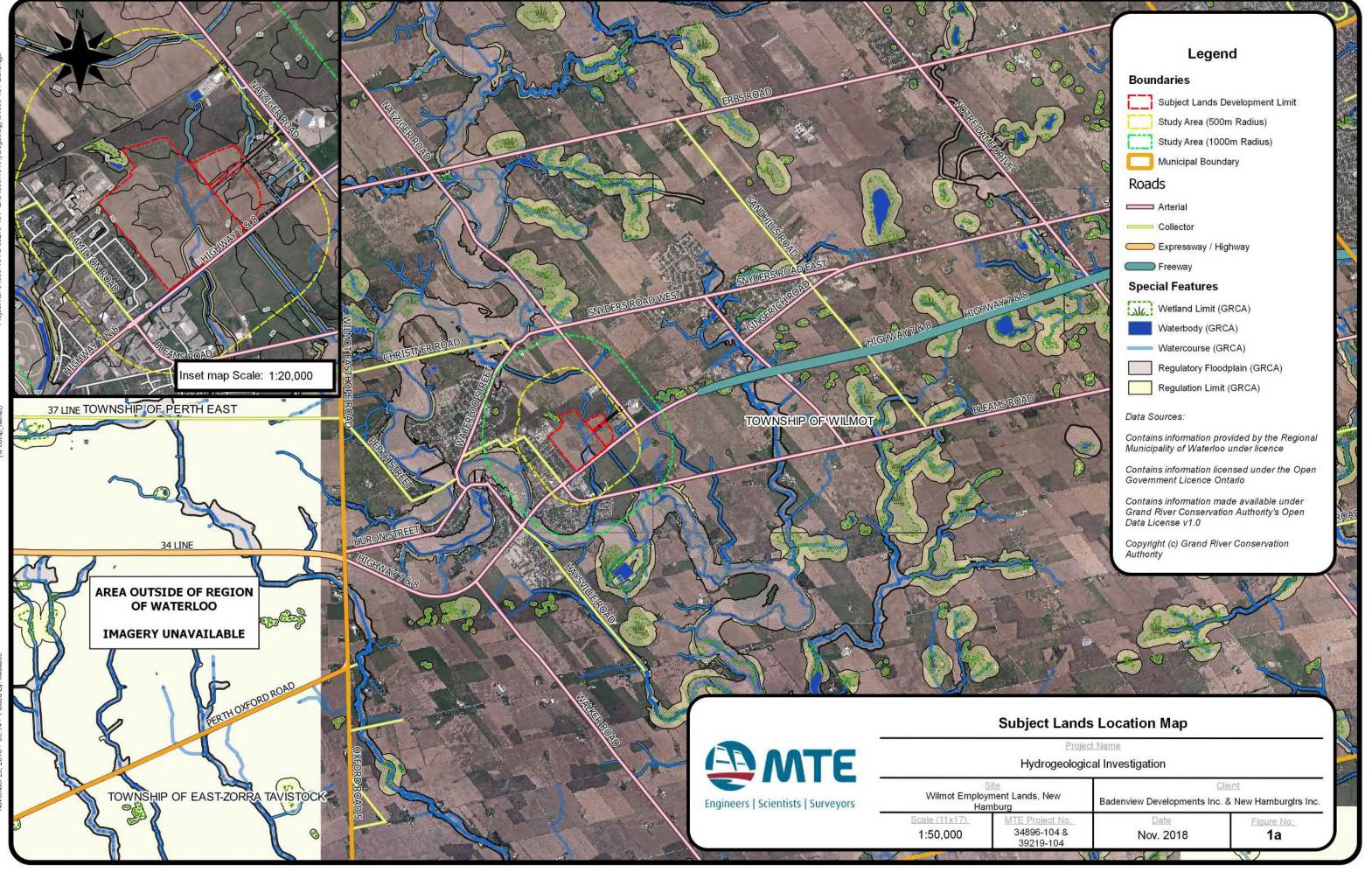
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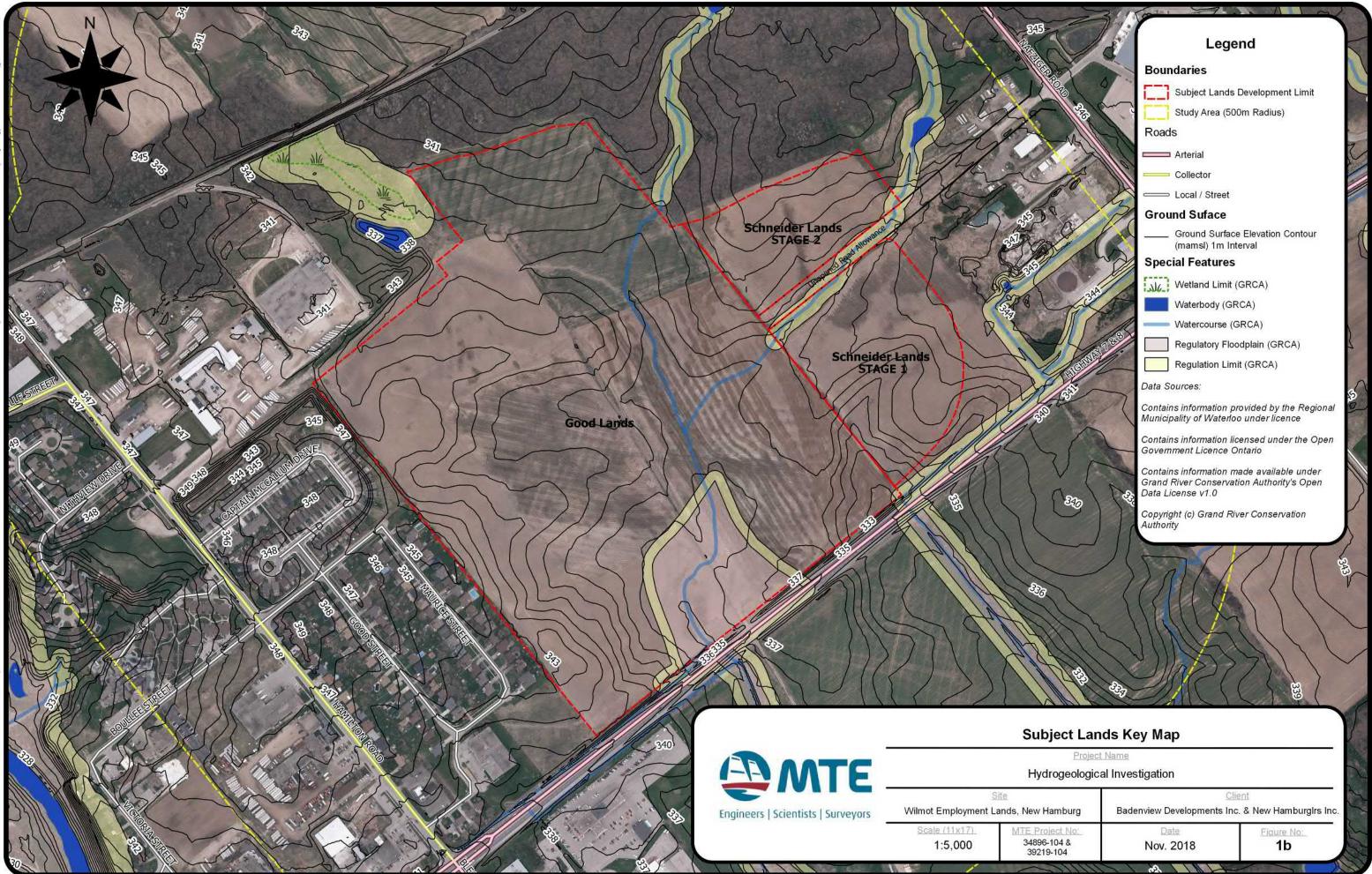


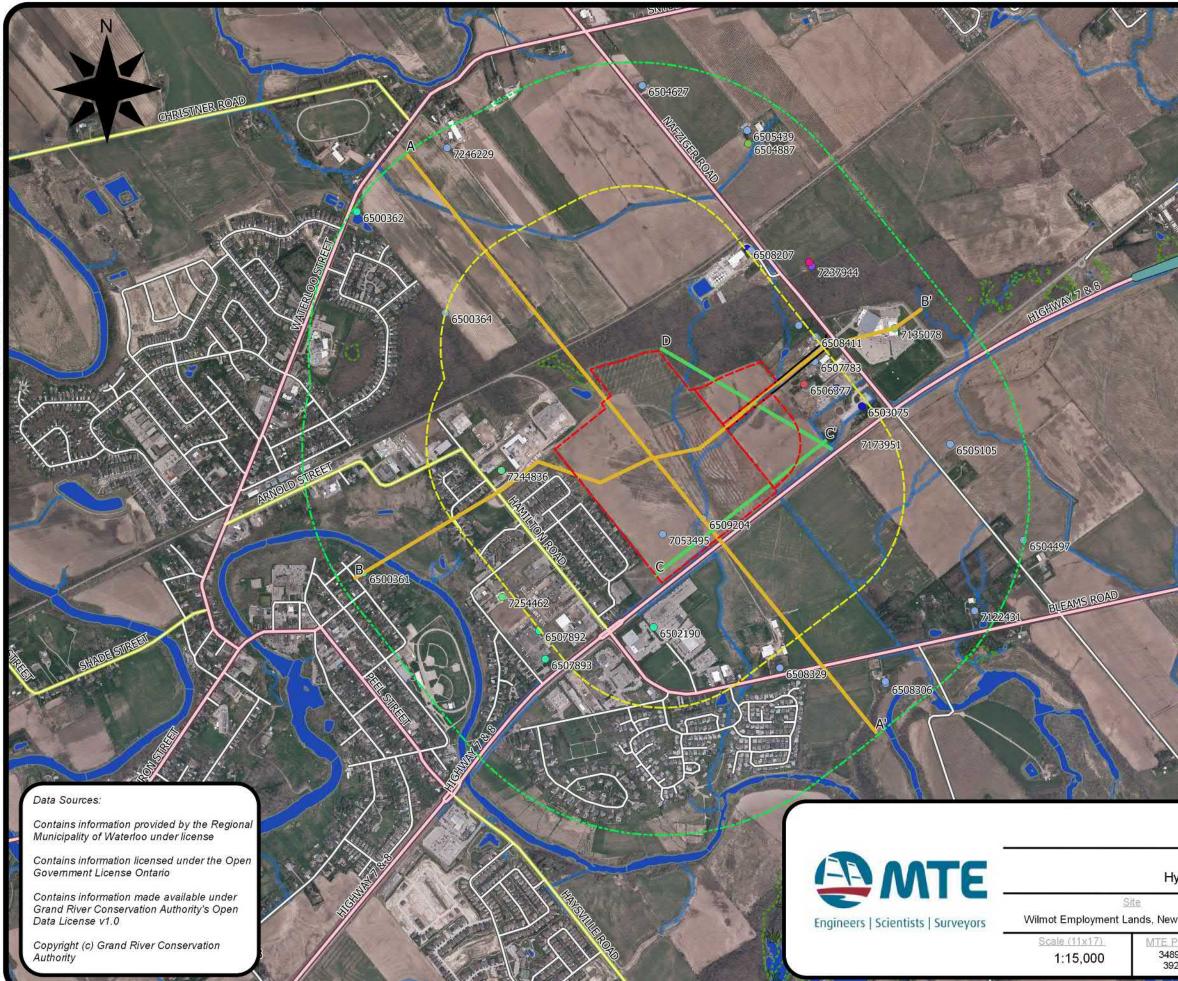
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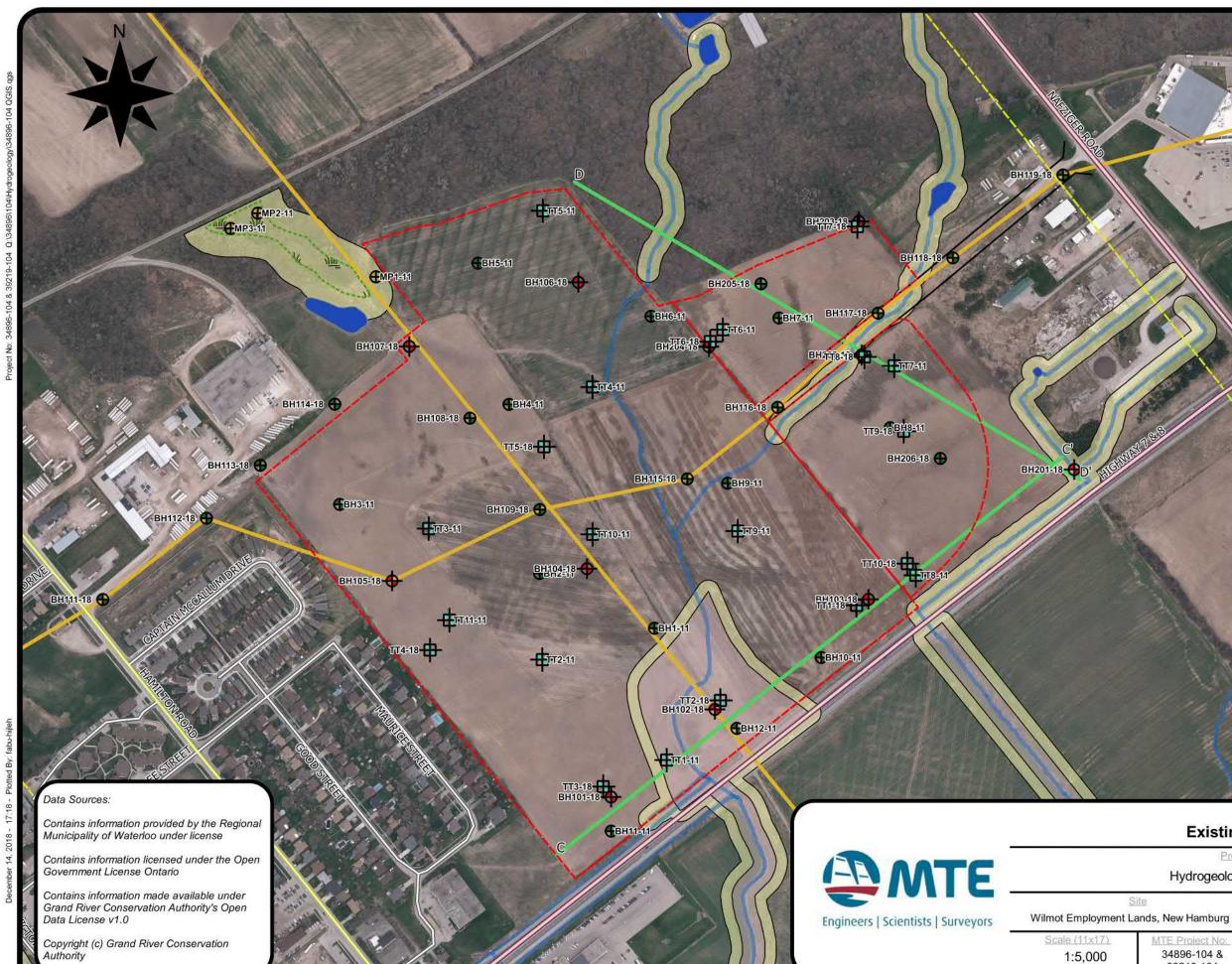
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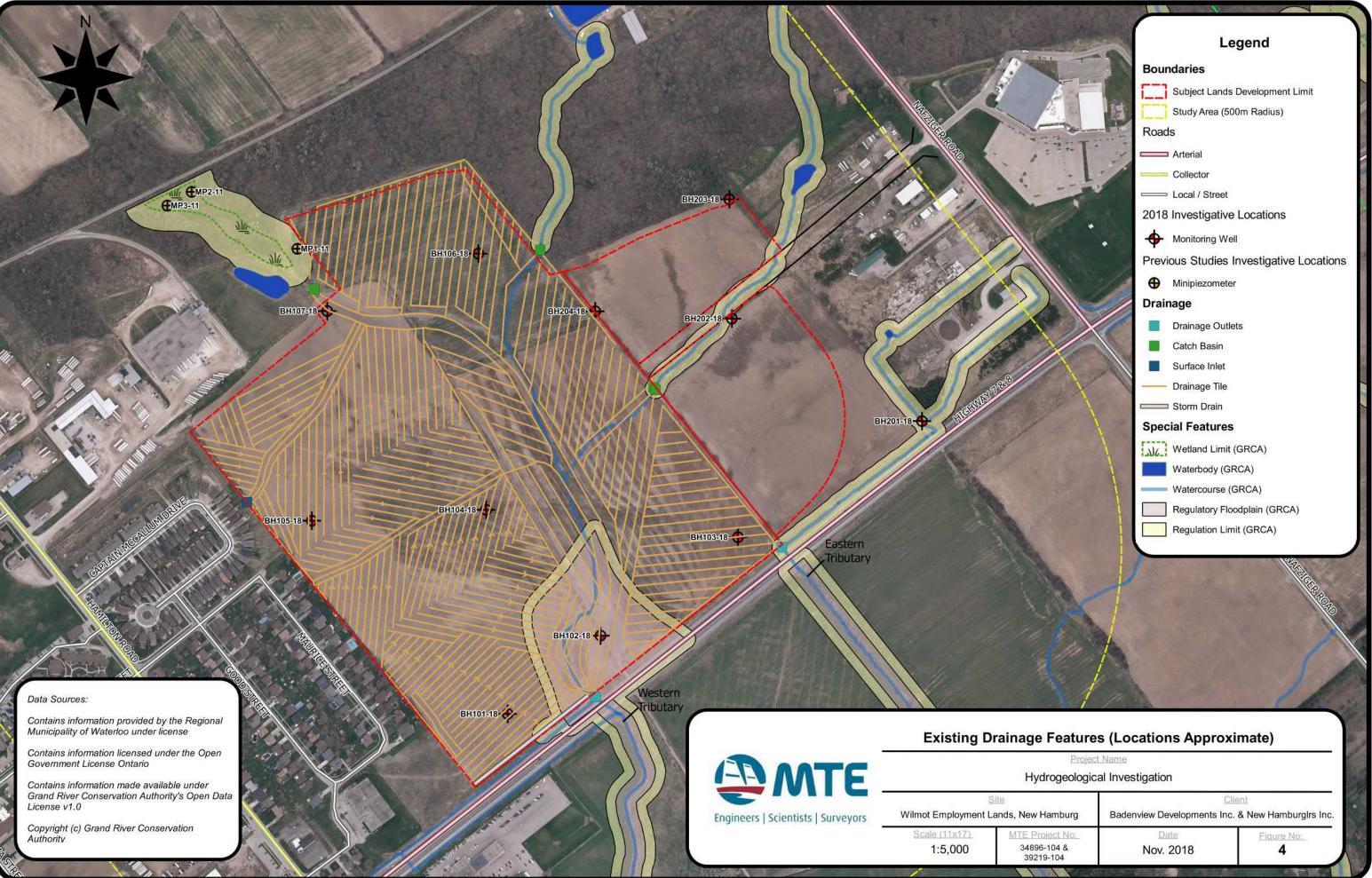


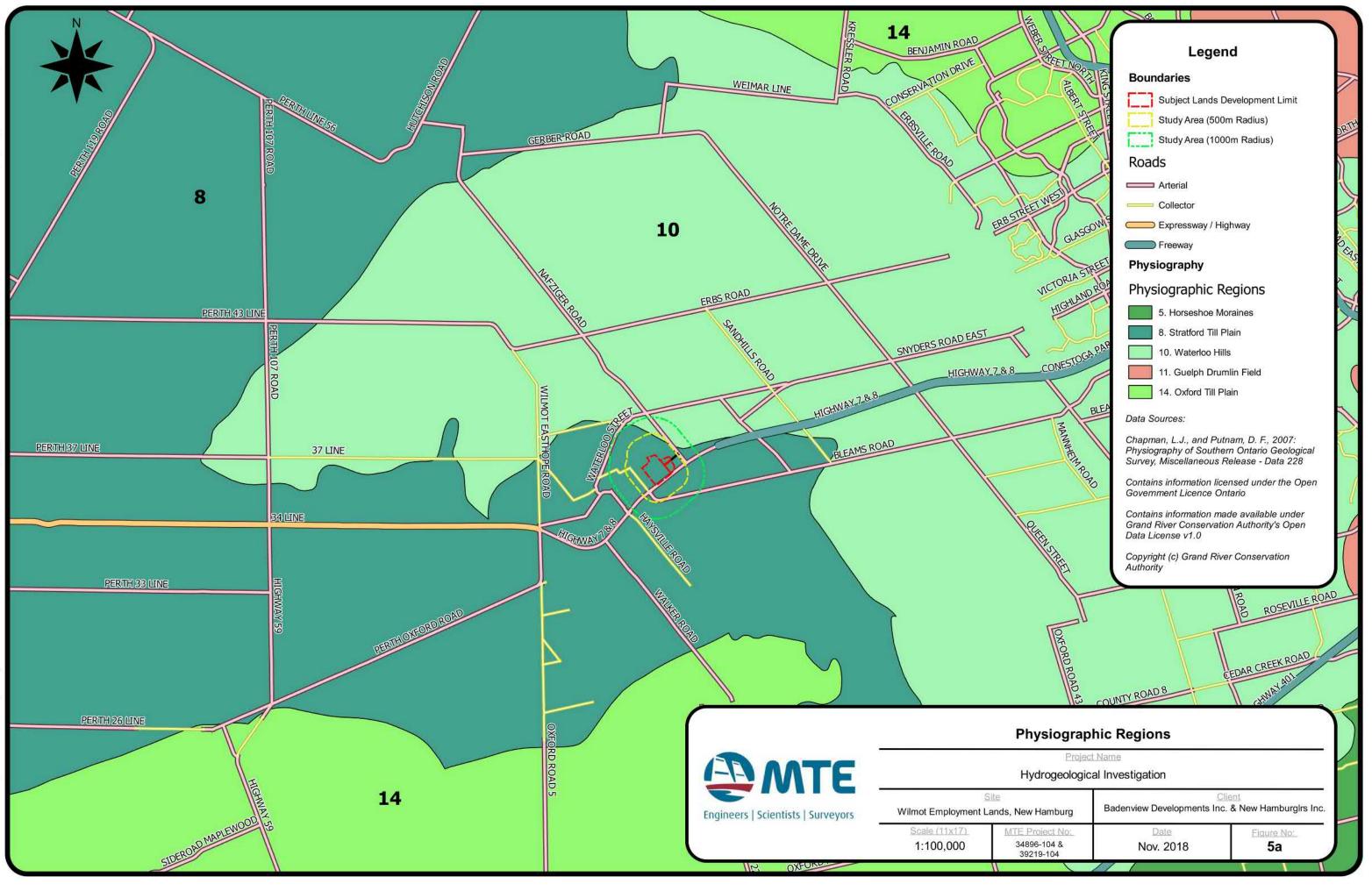


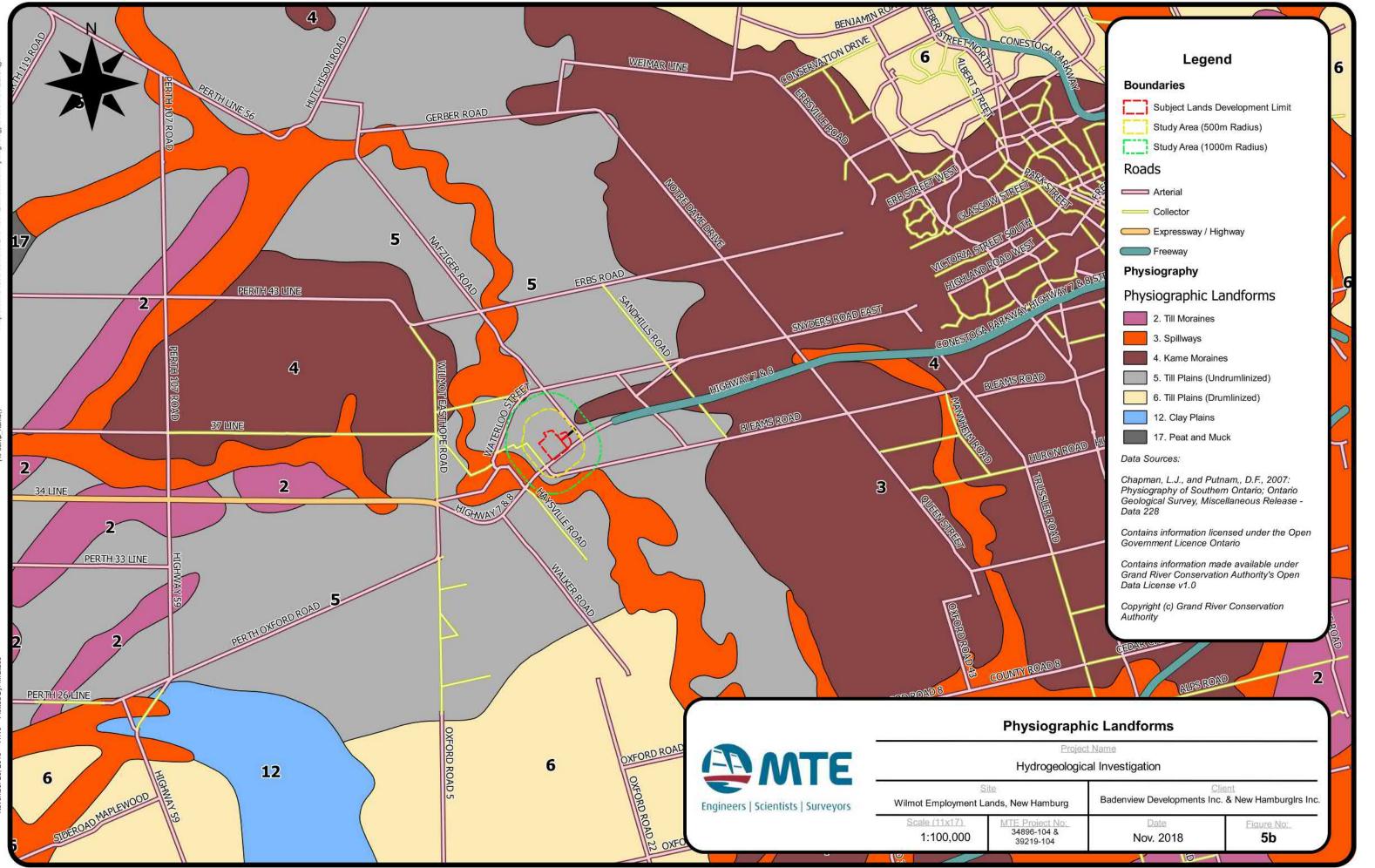
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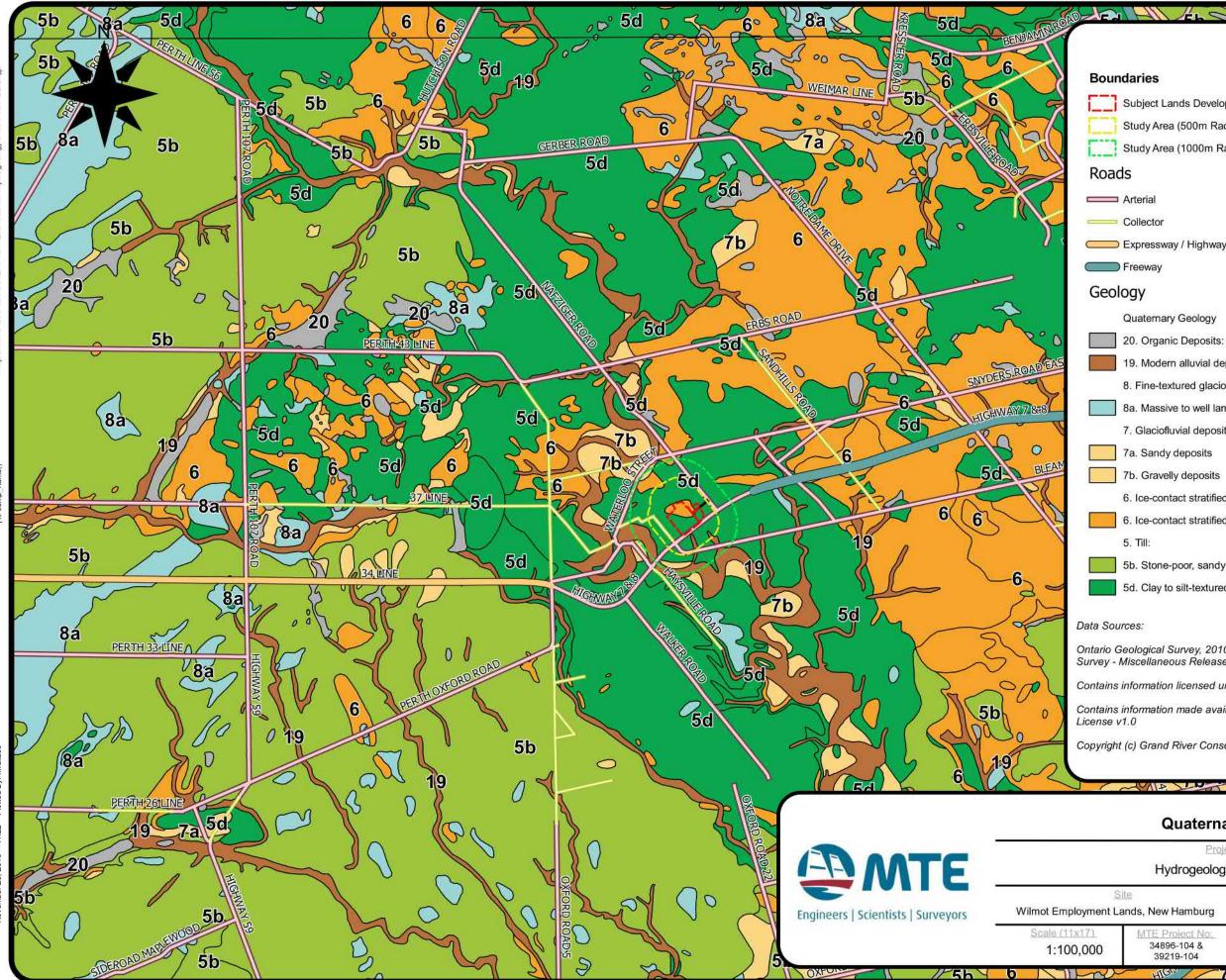












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Subject Lands Development Limit

EL OB

- Study Area (500m Radius)
- Study Area (1000m Radius)

- Quaternary Geology
- 20. Organic Deposits: peat, muck, marl
 - 19. Modern alluvial deposits: clay, silt, sand, gravel, may contain organic remains
 - 8. Fine-textured glaciolacustrine deposits: silt and clay, minor sand and gravel
- 8a. Massive to well laminated
 - 7. Glaciofluvial deposits: river deposits and delta topset facies
- 7a. Sandy deposits
- 7b. Gravelly deposits
- 6. Ice-contact stratified deposit: sand and gravel, minor silt, clay and till
- 6. Ice-contact stratified deposit: sand and gravel, minor silt, clay and till

5b. Stone-poor, sandy silt to silty sand-textured till on Paleozoic terrain

5d. Clay to silt-textured till (derived from glaciolacustrine deposits or shale)

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Quaternary Geology

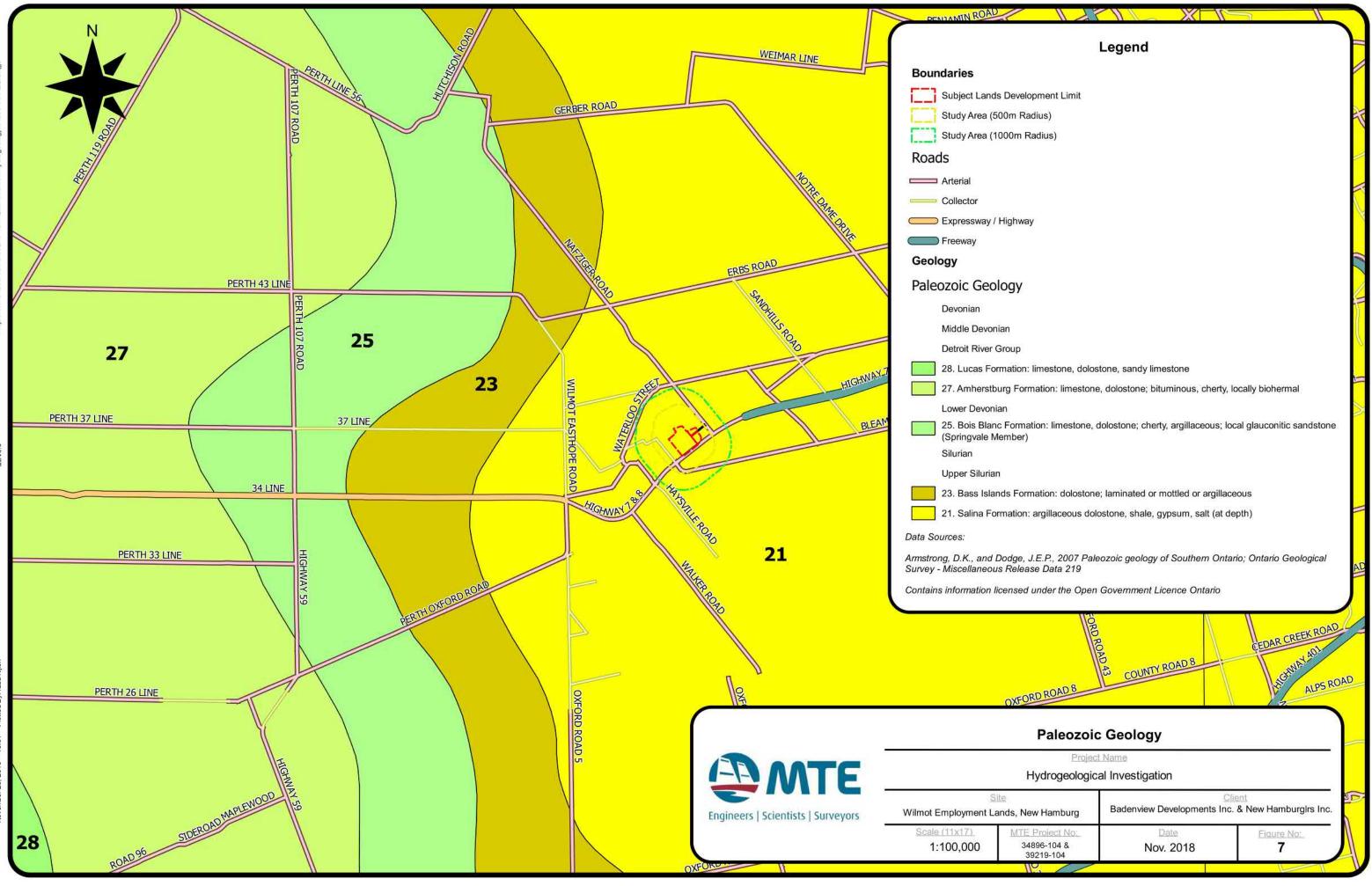
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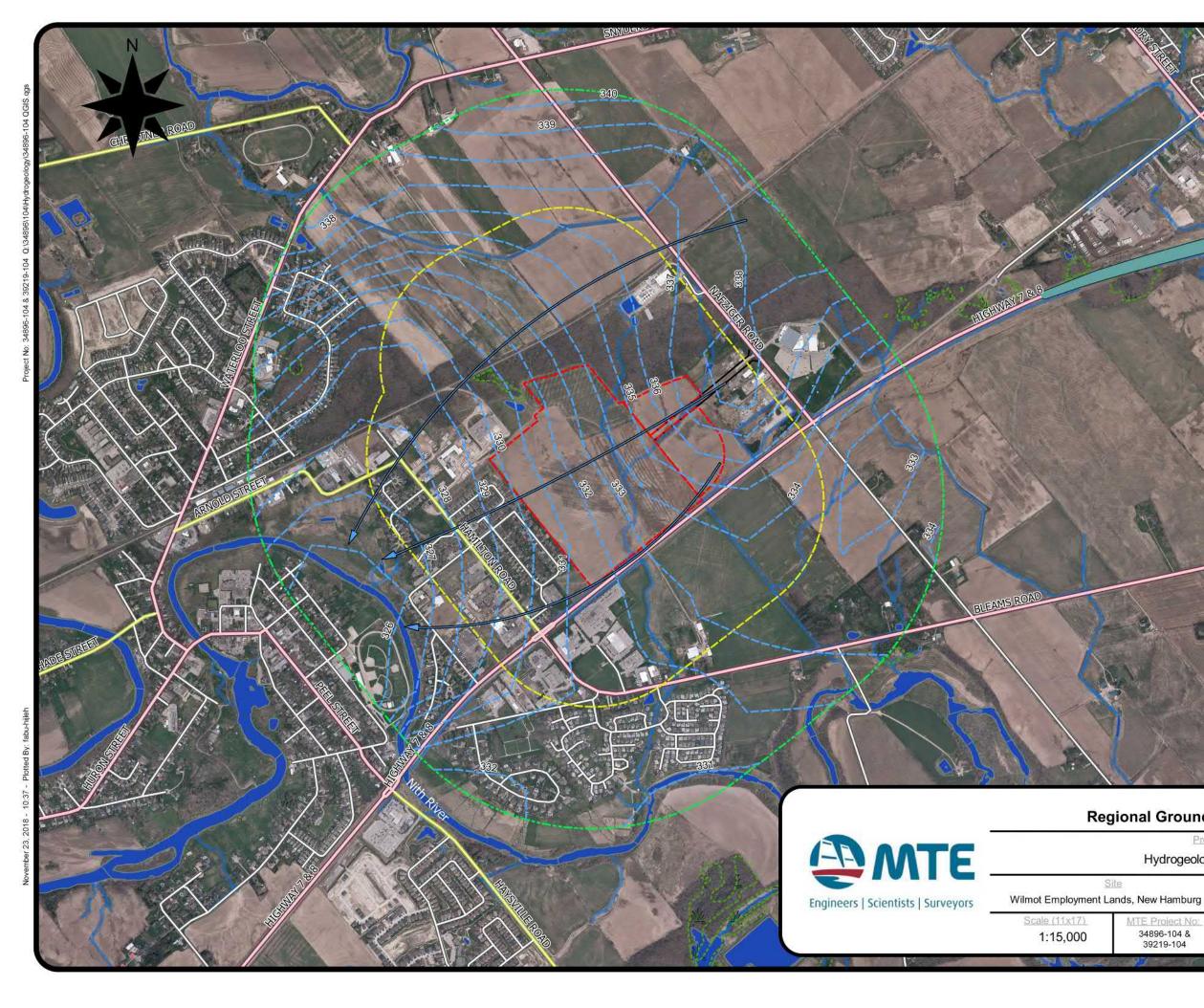
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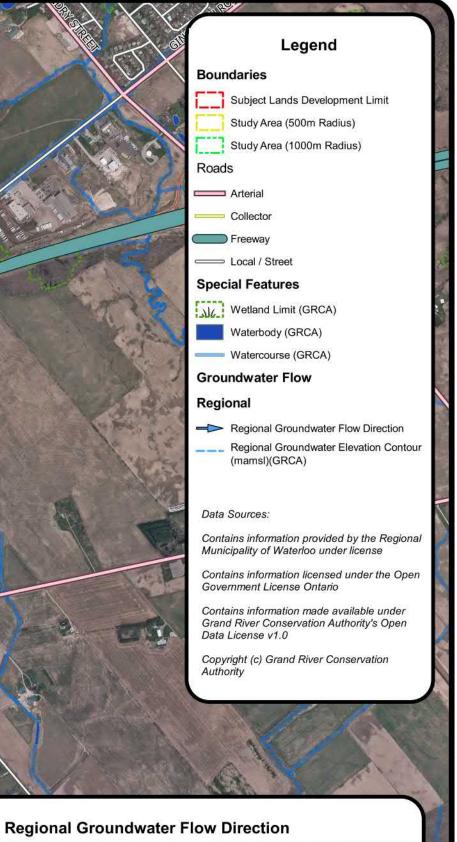
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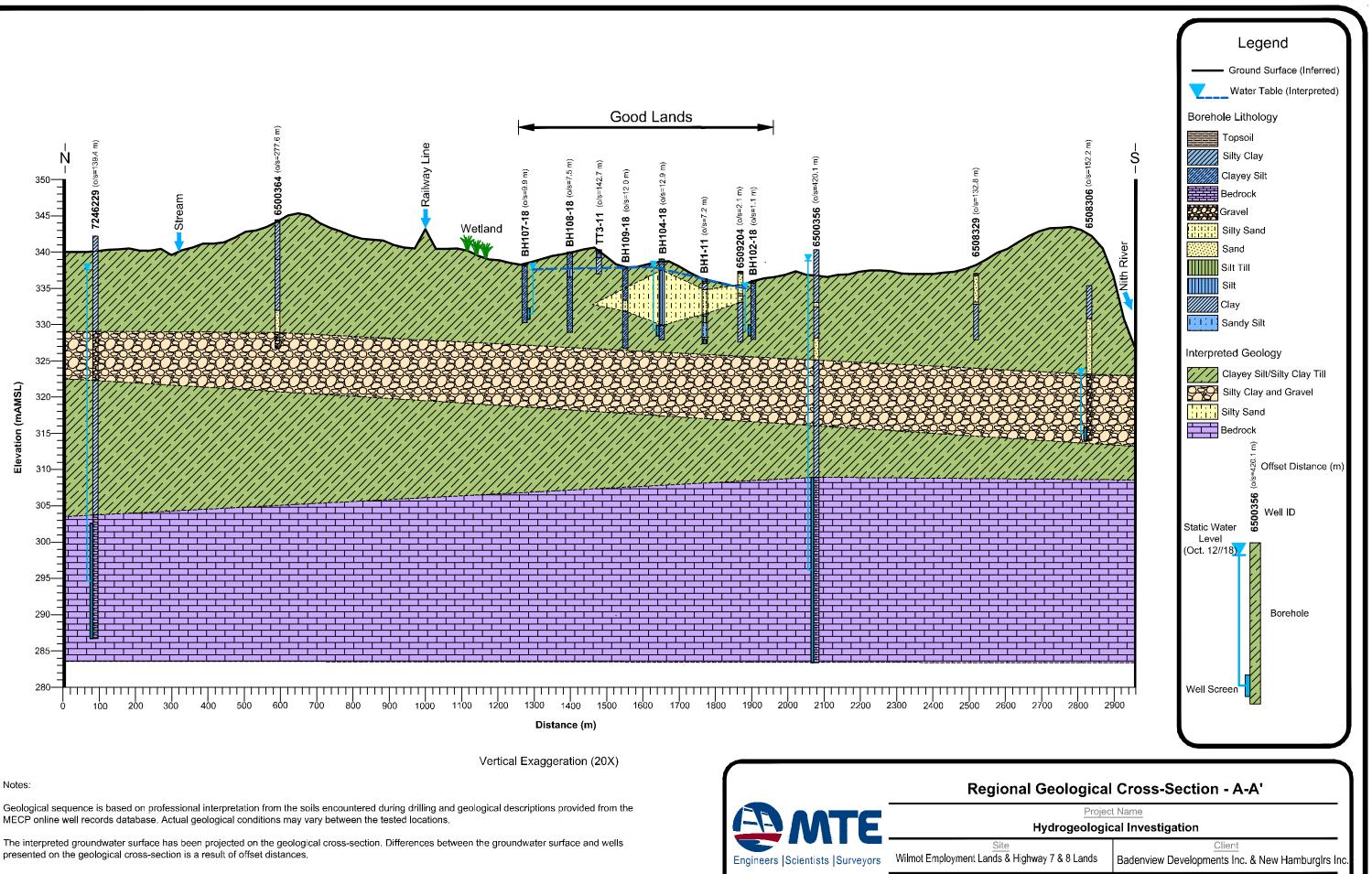
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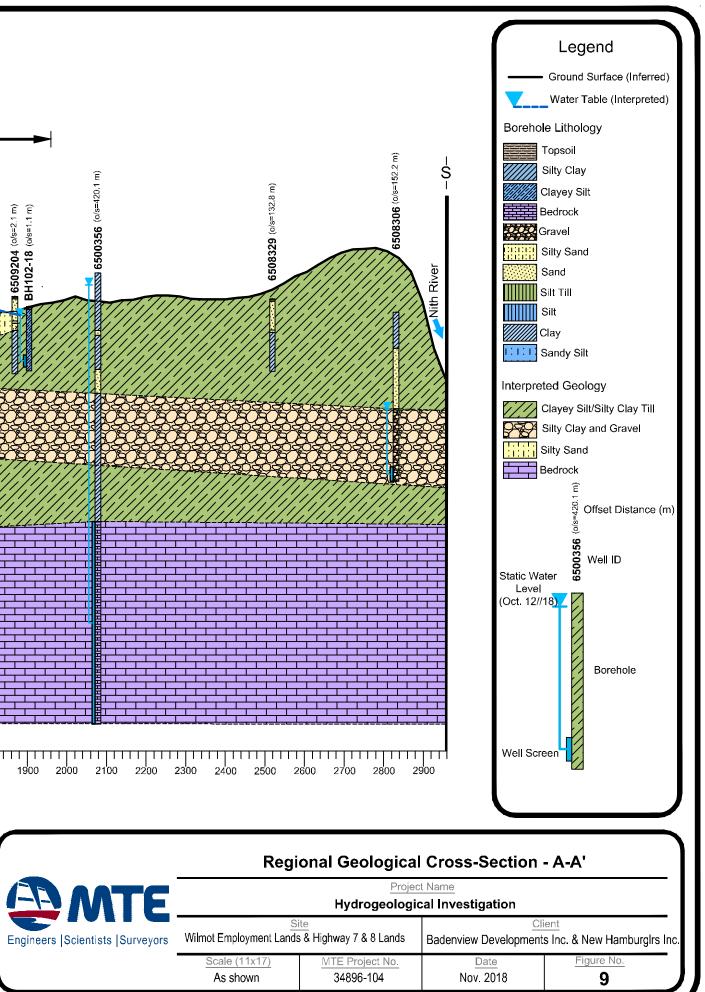


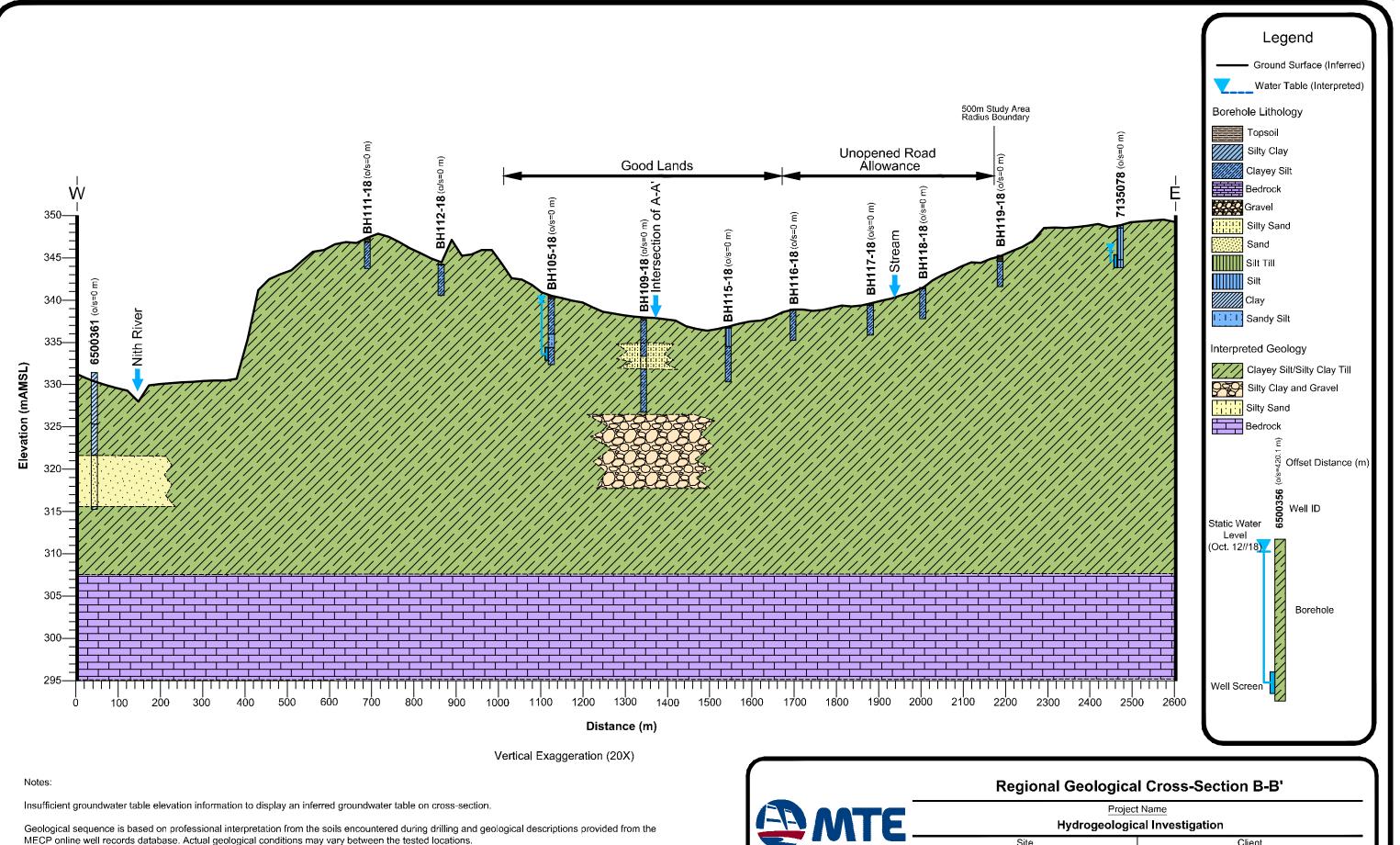




MECP online well records database. Actual geological conditions may vary between the tested locations.

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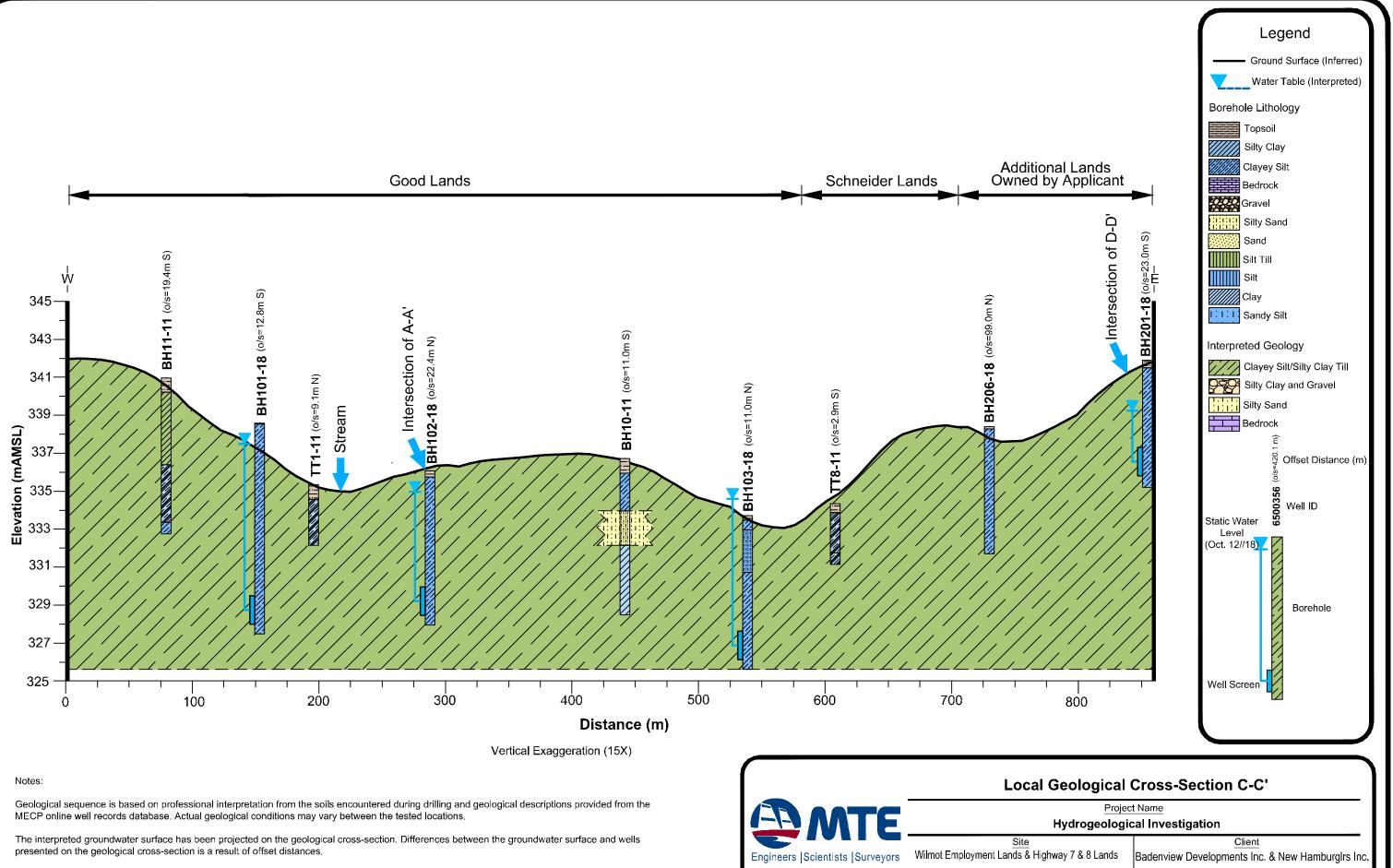




The interpreted groundwater surface has been projected on the geological cross-section. Differences between the groundwater surface and wells presented on the geological cross-section is a result of offset distances.

Engineers |Scientists |Surveyors

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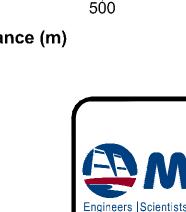
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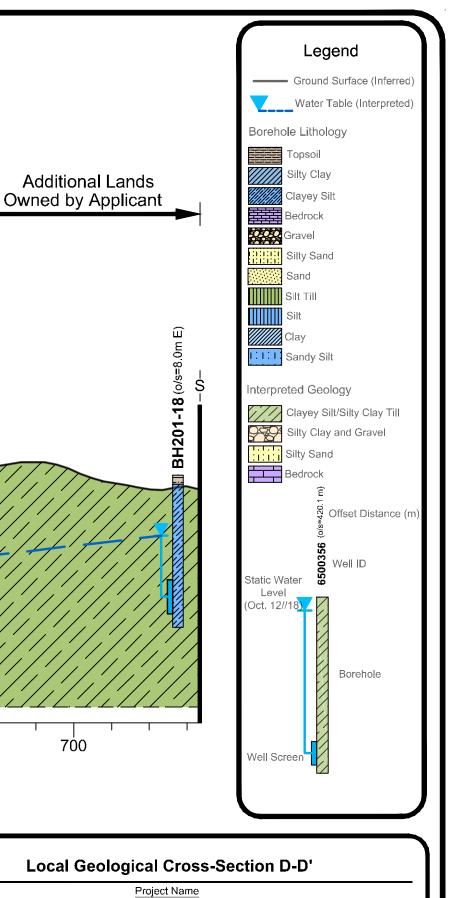
Geological sequence is based on professional interpretation from the soils encountered during drilling and geological descriptions provided from the MECP online well records database. Actual geological conditions may vary between the tested locations.

The interpreted groundwater surface has been projected on the geological cross-section. Differences between the groundwater surface and wells presented on the geological cross-section is a result of offset distances.

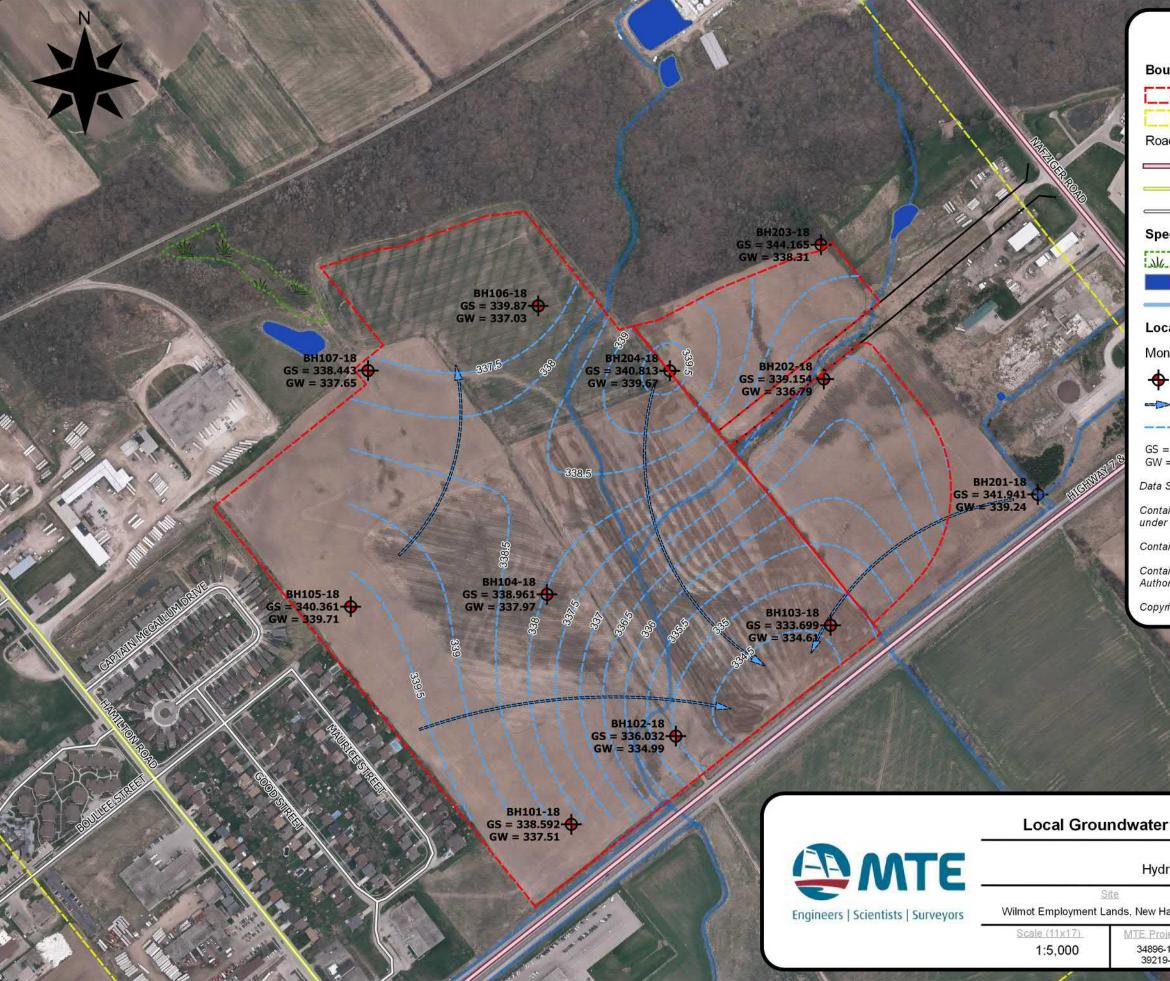


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Boundaries

- Subject Lands Development Limit Study Area (500m Radius)
- Roads
- Arterial
- Collector
- C Local / Street

Special Features

- Wetland Limit (GRCA)
- Waterbody (GRCA)
- Watercourse (GRCA)

Local Groundwater Flow

Monitoring Locations

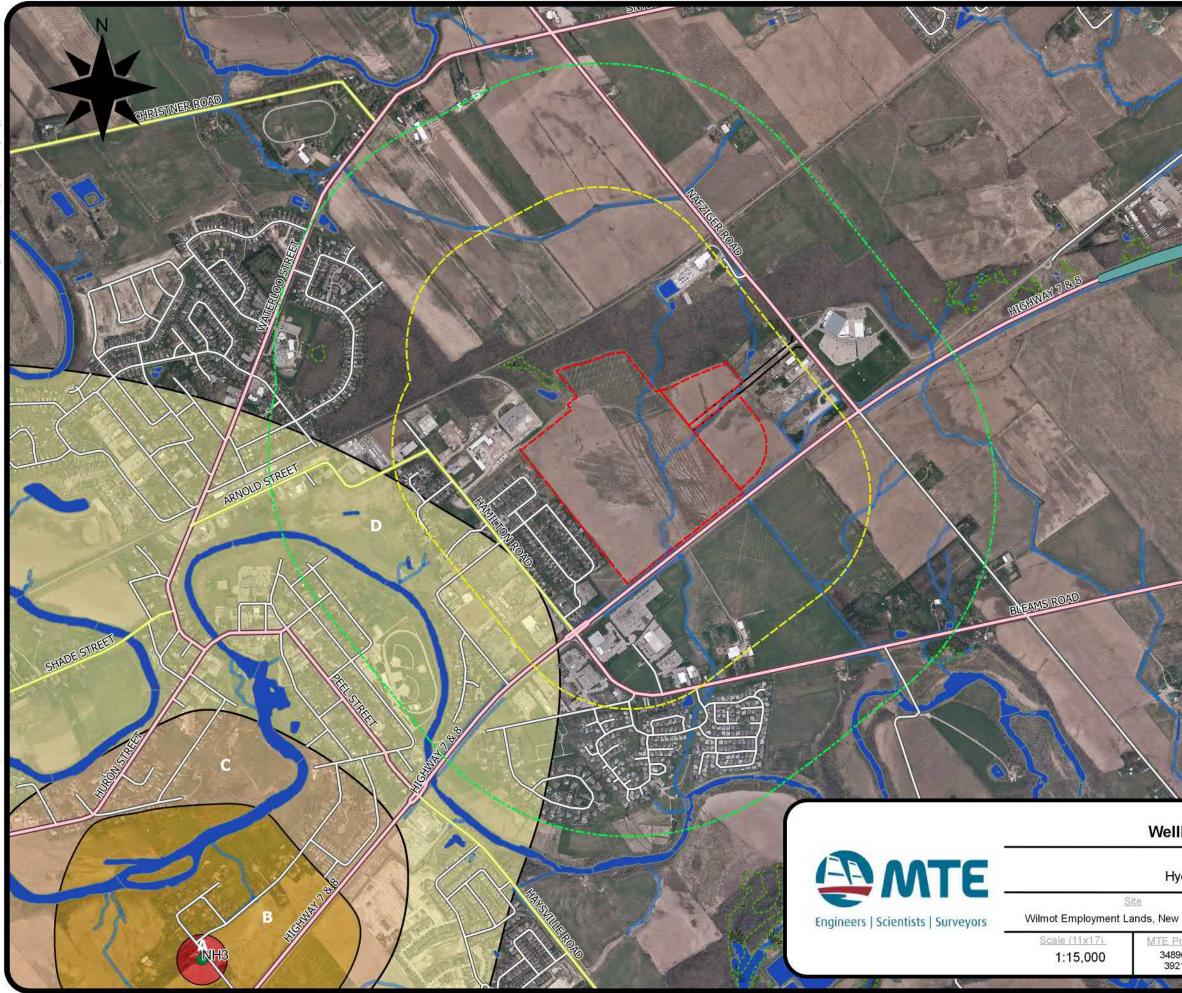
- Monitoring Well
- Local Groundwater Flow Direction Oct. 12, 2018
- ---- Local Groundwater Table Elevation Contour (mamsl) Oct. 12, 2018
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- Data Sources:
- Contains information provided by the Regional Municipality of Waterloo under license
- Contains information licensed under the Open Goverment License Ontario
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Local Groundwater Flow Interpretation - Oct. 12, 2018

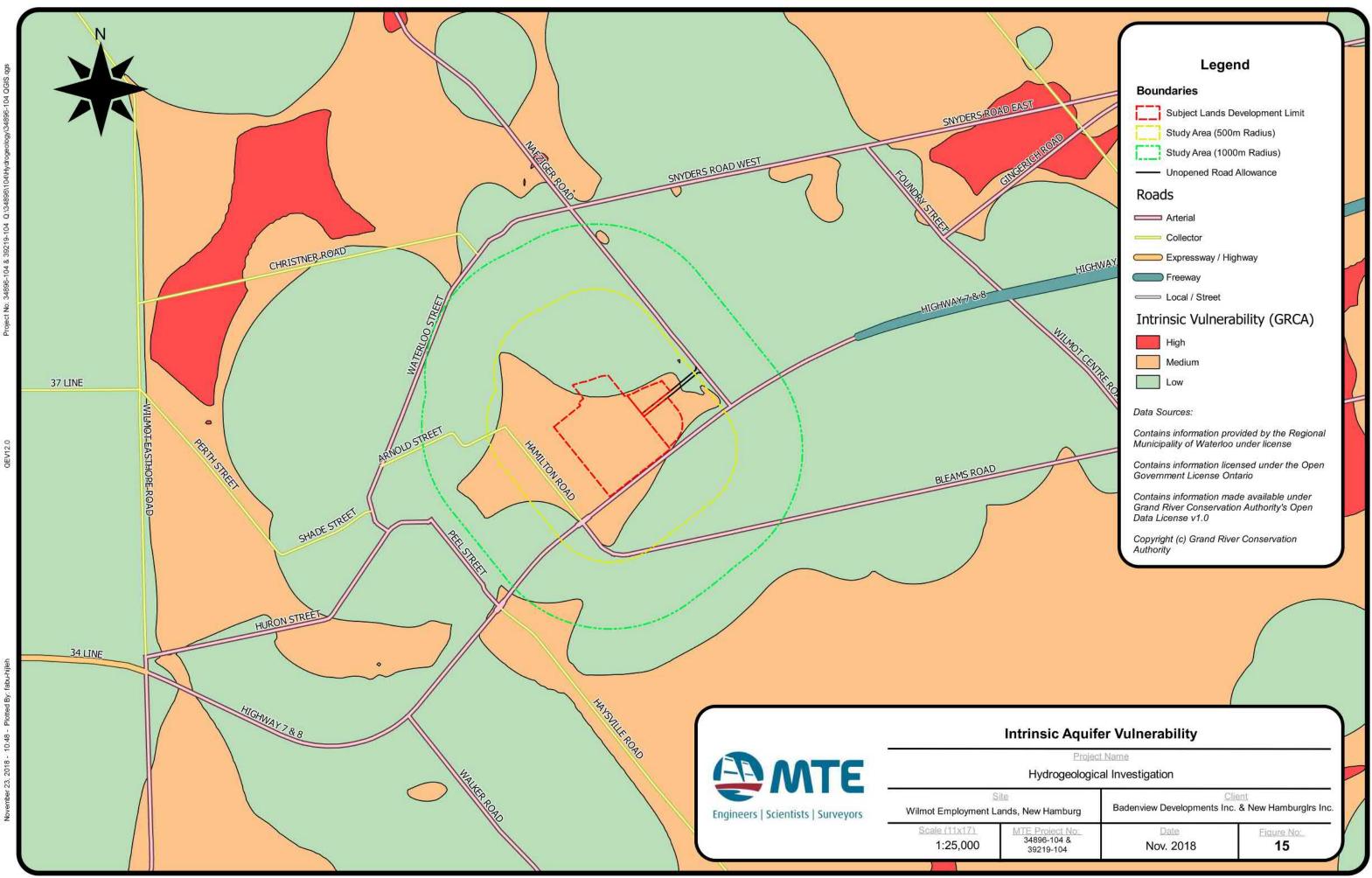
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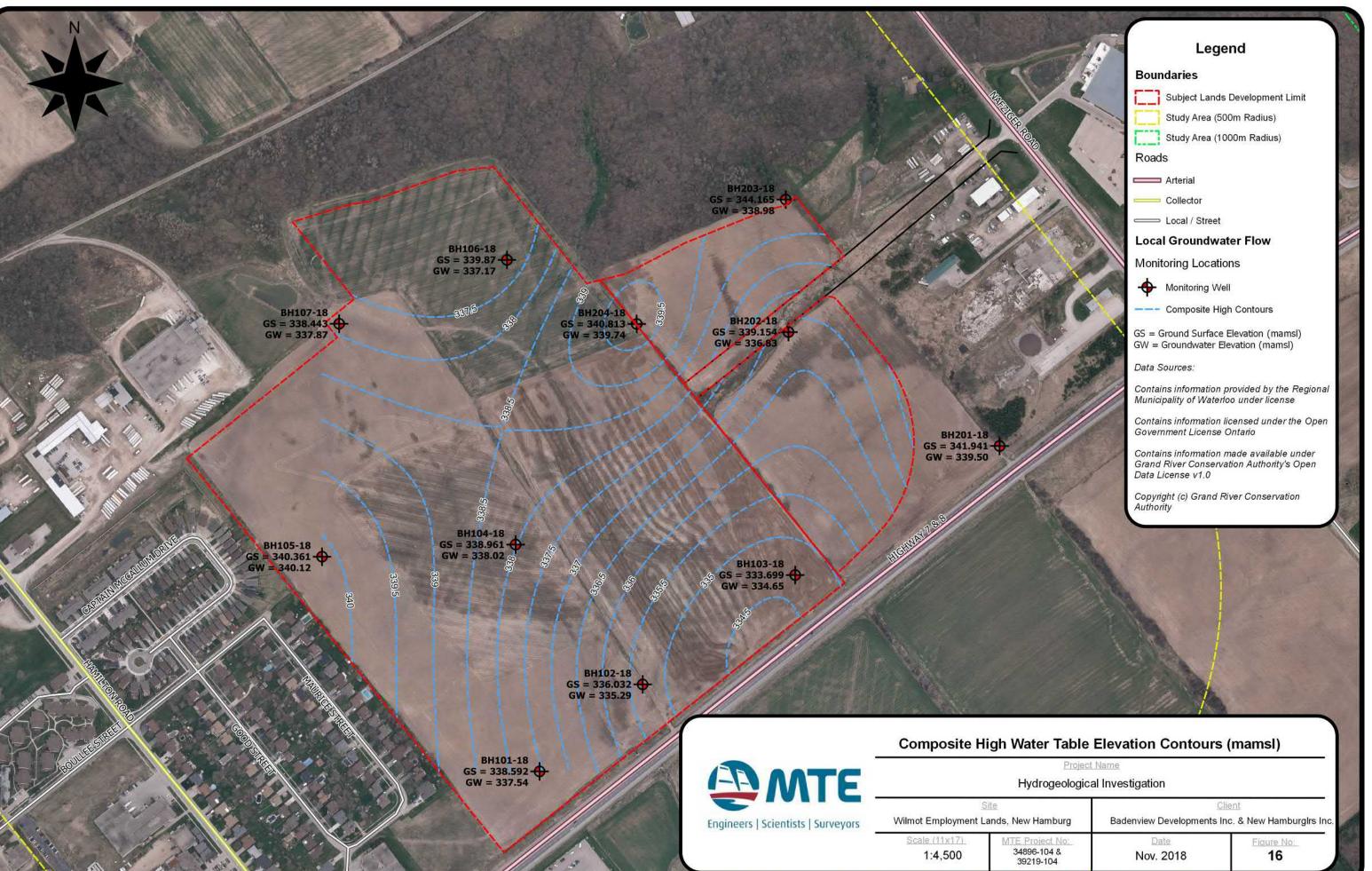
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7 <u>roiect No:</u> 96-104 & 219-104	Date Nov. 2018	Figure No: 14	a all





		Client					
lew Hamburg	Badenview Developments Inc. & New HamburgIrs Inc.						
E Project No:	Date	Figure No:					
4896-104 & 39219-104	Nov. 2018	16					



TABLES

Drawing on experience...Building on

gth.

ID	GOOD LANDS													
ID	BH10)1-18	BH10)2-18	BH10	03-18	BH10	04-18	BH105-18		BH106-18		BH107-18	
TOC Elevation (mAMSL)	339).44	336	5.79	334	1.64	339	9.74	341	27	340).75	339	.21
Stickup (m)	0.	84	0.	76	0.	94	0.	78	0.	91	0.	88	0.1	77
Date	mbtoc	mbgs	mbtoc	mbgs	mbtoc	mbgs	mbtoc	mbgs	mbtoc	mbgs	mbtoc	mbgs	mbtoc	mbgs
8-Apr-18	1.87	1.03	1.65	0.89	7.632	6.69	1.45	0.67	1.65	0.74	3.585	2.71	1.36	0.59
10-Apr-18	1.87	1.03	1.74	0.98	7.55	6.61	1.50	0.72	nm	-	3.65	2.77	1.45	0.68
13-Apr-18	1.92	1.08	1.825	1.07	7.44	6.50	1.53	0.75	1.61	0.70	3.56	2.68	1.52	0.75
16-Apr-18	1.86	1.02	nm	-	nm	-	1.33	0.55	1.08	0.17	nm	-	1.23	0.46
2-May-18	1.812	0.98	1.885	1.13	7.28	6.34	1.64	0.86	1.64	0.73	3.545	2.67	1.53	0.76
16-May-18	1.93	1.10	2.00	1.24	5.50	4.56	1.86	1.08	1.76	0.85	3.59	2.71	1.65	0.88
1-Jun-18	2.37	1.53	2.27	1.51	2.93	1.99	2.80	2.02	2.60	1.69	3.60	2.72	2.15	1.38
17-Jul-18	3.96	3.12	2.89	2.13	0.32	-0.62	4.26	3.48	4.01	3.10	nm	-	3.50	2.73
20-Jul-18	nm	-	nm	-	nm	-	nm	-	nm	-	3.76	2.88	nm	-
10-Aug-18	nm	-	nm	-	nm	-	nm	-	nm	_	nm	-	nm	-
10-Oct-18	nm	-	nm	-	nm	-	nm	_	nm	_	nm	-	nm	-
12-Oct-18	1.93	1.09	1.80	1.04	0.025	-0.92	1.77	0.99	1.56	0.65	3.72	2.84	1.56	0.79

ID				SCHNEID	ER LANDS				
ID	BH20)1-18	BH2	02-18	BH2	03-18	BH204-18		
TOC Elevation (mAMSL)	342	.73	339	9.91	345	5.01	341.58		
Stickup (m)	0.	79	0.	76	0.	84	0.	76	
Date	mbtoc	mbgs	mbtoc	mbgs	mbtoc	mbgs	mbtoc	mbgs	
8-Apr-18	ni	-	ni	-	ni	-	ni	-	
10-Apr-18	ni	-	ni	-	ni	-	ni	-	
13-Apr-18	ni	-	ni	-	ni	-	ni	-	
16-Apr-18	ni	-	ni	-	ni	-	ni	-	
2-May-18	ni	-	ni	-	ni	-	ni	-	
16-May-18	ni	-	ni	-	ni	-	ni	-	
1-Jun-18	ni	-	ni	-	ni	-	ni	-	
17-Jul-18	ni	-	ni	-	ni	-	ni	-	
20-Jul-18	ni	-	ni	-	ni	-	ni	-	
10-Aug-18	3.955	3.17	3.18	2.42	6.31	5.47	2.27	1.51	
10-Oct-18	3.27	2.48	3.15	2.39	6.3	5.46	1.92	1.16	
12-Oct-18	3.49	2.70	3.12	2.36	6.7	5.86	1.91	1.15	

Notes:

nm = not measured

ni = not installed

TOC = Top of Casing

mAMSL = meters above mean sea level

mbtoc = meters below top of casing

Monitoring well TOC and Ground Surface elevations surveyed October 29, 2018

Table 2. Groundwater Elevations (mAMSL)

ID				GOOD LANDS					SCHNEID	ER LANDS	
ID	BH101-18	BH102-18	BH103-18	BH104-18	BH105-18	BH106-18	BH107-18	BH201-18	BH202-18	BH203-18	BH204-18
TOC Elevation (mAMSL)	339.44	336.79	334.64	339.74	341.27	340.75	339.21	342.73	339.91	345.01	341.58
Stickup (m)	0.84	0.72	0.90	0.69	0.79	0.82	0.81	0.82	0.86	0.80	0.78
GS Elevation (mAMSL)	338.59	336.03	333.70	338.96	340.36	339.87	338.44	341.94	339.15	344.17	340.81
8-Apr-18	337.57	335.14	327.01	338.29	339.63	337.16	337.85	-	-	-	-
10-Apr-18	337.57	335.05	327.09	338.24	-	337.10	337.76	-	-	-	-
13-Apr-18	337.52	334.97	327.20	338.21	339.67	337.19	337.69	-	-	-	-
16-Apr-18	337.58	-	-	338.41	340.19	-	337.98	-	-	-	-
2-May-18	337.62	334.91	327.36	338.10	339.64	337.20	337.68	-	-	-	-
16-May-18	337.50	334.79	329.14	337.88	339.51	337.16	337.56	-	-	-	-
1-Jun-18	337.07	334.52	331.71	336.94	338.67	337.15	337.06	-	-	-	-
17-Jul-18	335.48	333.90	334.32	335.48	337.26	-	335.71	-	-	-	-
20-Jul-18	-	-	-	-	-	336.99	-	-	-	-	-
10-Aug-18	-	-	-	-	-	-	-	338.77	336.73	338.70	339.31
10-Oct-18	-	-	-	-	-	-	-	339.46	336.76	338.71	339.66
12-Oct-18	337.51	334.99	334.61	337.97	339.71	337.03	337.65	339.24	336.79	338.31	339.67

Notes:

TOC = Top of Casing

mAMSL = meters above mean sea level

Table 3. Mini-Piezometer Water Elevations and Vertical Hydraulic Gradients

	Location	М	P1	М	P2	М	Р3
Date	TOC Elevation	339	9.61	340	.181	340.366	
		mbtoc	mamsl	mbtoc	mamsl	mbtoc	mamsl
-18	Inside Level (IL) (m)	0.98	338.63	0.64	339.541	0.60	339.769
16-May	Outside Level (OL) (m)	0.98	338.63	0.64	339.541	0.6	339.769
16-	Vertical Hydraulic Gradient (m/m)	0	-	0	-	0.0	-
18	Inside Level (IL) (m)	1.49	338.12	0.835	339.346	0.62	339.746
1-Jun-:	Outside Level (OL) (m)	dry	-	dry	-	0.62	339.746
, -	Vertical Hydraulic Gradient (m/m)	-	-	-	-	0.0	-
.18	Inside Level (IL) (m)	1.015	338.60	0.782	339.40	0.61	339.756
-Oct-	Outside Level (OL) (m)	dry	-	dry	-	0.61	339.756
12-	Vertical Hydraulic Gradient (m/m)	-	-	-	-	0.0	340.366

Notes:

TOC = Top of Casing

mAMSL = meters above mean sea level

mbtoc = meters below top of casing

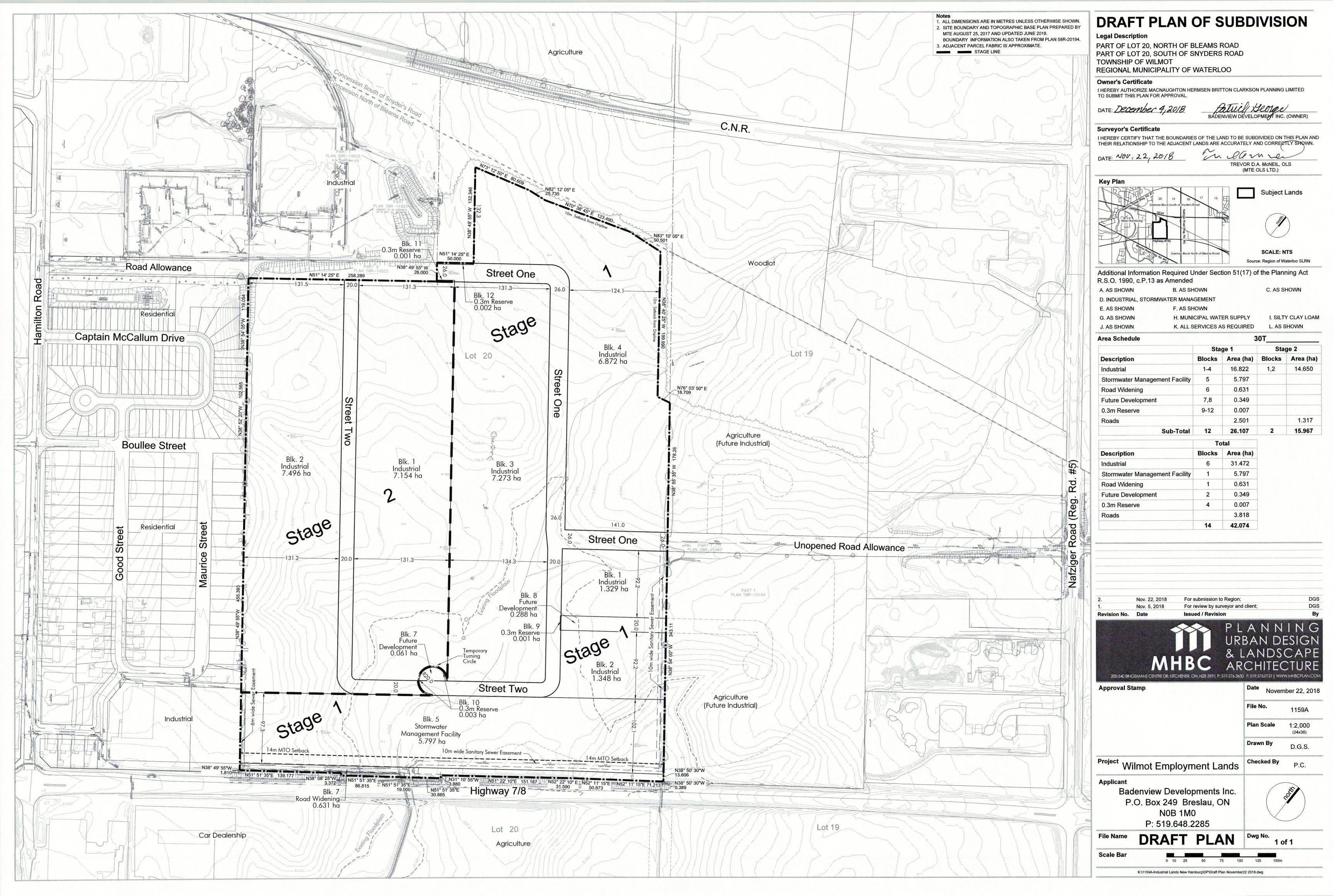


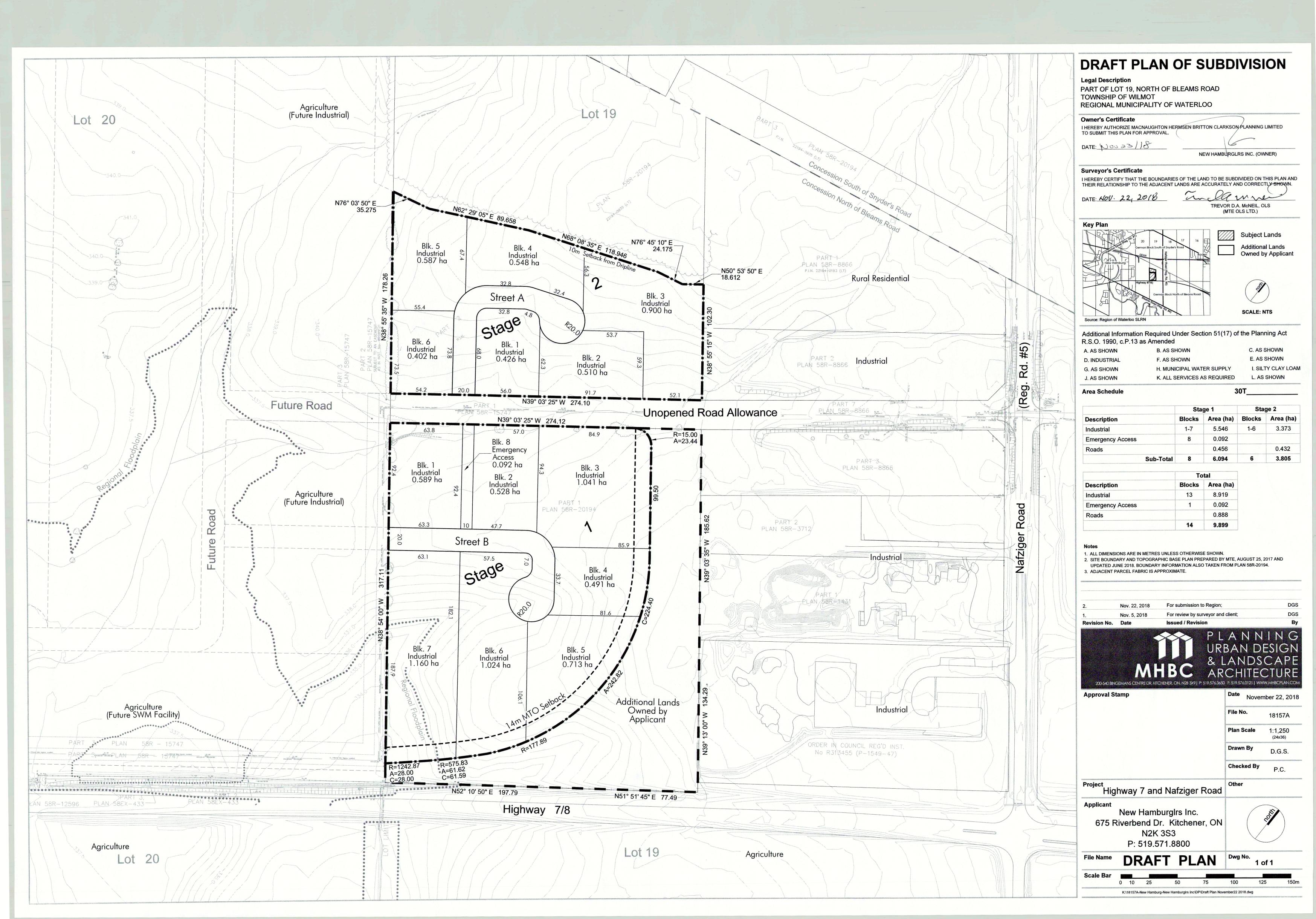
APPENDIX A

DRAFT PLAN OF SUBDIVISION

Drawing on experience...Building on

gth.







APPENDIX B

BOREHOLE LOGS

Drawing on experience...Building on

gth.

Project: Hydrogeological Investigations

Location: Wilmot lands

Borehole Number: BH1

Job Number: 34896-100

Drill Date: November 29, 2010

Depth (m)	Elevation (m)	Soil Description	Symbol	Number	Type	N-Value	Standard Penetration Graph	Headspace (ppm)	Borehole
0.0 <u>ft m</u> 0.0	0.00 0.00	Ground Elevation TOPSOIL	~~			ł		4	
2.0	-0.61 0.61	SILT_CLAY	\sim						
4.0	-1.52	Light brown sandy silt and clay, fine grained, loose, moist, no staining or odour	Ţ	1	ss	21	\mathbf{X}		
6.0	1.52	Silty SAND Light brown silty sand, some clay @ 6', fine grained, stiff,		2	SS	40			
2.0 4.0 6.0 10.0 8.0 10.0 12.0		moist to wet @ 7', saturated below 7', no staining or odour		3	SS	55			
10.0				4	SS	75	$\langle \rangle$		
- 4.0									
14.0	-4.88 4.88	Sandy SILT		5	SS	63			
18.0	-6.10 6.10	Grey sandy silt, trace clay, fine grained, stiff, saturated SILT TILL Grey sandy silt till, small stones, no staining or odour							
2.0		Sandy SILT Light grey sandy silt, some silty clay @ 22', fine grained, stiff, no staining or odur, wet, dry @ 22'		6	SS	51			
6.0 - 8.0	-8.08 8.08	CLAY		7	SS	31			
28.0	-8.99	Grey clay, trace silt, dry, no staining or odour SILT		8	SS	39			
	8.99	Grey silt, fine grained, dry							
32.0 1 10.0									
Reviewe Method: Notes:	-	RBM v Stem Auguring/Split Spoon		Bingen Kitche N	n suitar nans Ce ener, Or I2B 3X9	entre D Itario			gged By: YXM eet: 1 of 1
110163.				(519) 743-6	500		Sh	.

Project: Hydrogeological Investigations

Location: Wilmot lands

Borehole Number: BH2

Job Number: 34896-100

Drill Date: November 30, 2010

Depth (m)	Elevation (m)	Soil Description	Symbol	Number	Type	N-Value	Standard Penetration Graph 25 50 75	Headspace (ppm)	Borehole
0.0 <u>ft m</u> 0.0	0.00	Ground Elevation TOPSOIL	~ ~						
.0	-0.61 0.61		$\sim\sim$				0		
€0. €0. €0. €0. 2.	0.01	SILT Light brown clayey silt, fine grained, stiff, dry, no staining or odour. Light brown sandy	T	1	SS	30			
0 + 2.0	-2.29	silt @ 7'	1	2	SS	51			
0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2.29 -3.05 3.05	Silty CLAY Grey-brown silty clay, fine grained, stiff, dry, no staining or odour	H	3	SS	42			
	3.05	CLAY Grey clay, fine, stiff, dry, trace		4	SS	23			
		sand @ 17', no staining or odour							
0 Internation				5	SS	33			
րորովորորդորդորդորորդորոր 6.				6	SS	27			
8.0	-8.23 8.23			7	SS	31			
դրերրությունը 10°0									
Reviewo Method Notes:		RBM v Stem Auguring/Split Spoon		Bingen Kitche N	nsultai nans Ce ener, Or I2B 3X9) 743-6	entre D ntario			gged By: YXM eet: 1 of 1

Project: Hydrogeological Investigations

Location: Wilmot lands

Borehole Number: BH3

Job Number: 34896-100

Drill Date: November 30, 2010

Depth (m)	Elevation (m)	Soil Description	Symbol	Number	Type	N-Value	Standard Penetration Graph	Headspace (ppm)	Borehole
0.0 ^{ft} m 0.0	0.00 0.00	Ground Elevation TOPSOIL	~~						
2.0	-0.61 0.61	SILT	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~						
4.0	-1.52	Light brown clayey silt, trace sand, dry, no staining or odour		1	SS	31			
6.0 2.0	1.52	Sandy SILT Light brown sandy silt with clay, fine grained, stiff, dry,		2	SS	49			
8.0 	2.05	slightly moist @ 8'		3	ss	38			
10.0	-3.05 3.05 -3.66 3.66	Silty CLAY Grey silty clay with sand, fine grained, stiff, dy, no staining or		4	ss	32			
14.0	3_00	odour Silty SAND Grey silty sand, trace clay							
		seams, fine grained, stiff, no staining or odour, dry to wet		5	SS	45			
18.0 19.0 19.0				6	SS	20			
22.0 11 24.0				0		20			
26.0 8.0	-8.23			7	SS	54	$ \rangle$		
	8.23								
30.0 1 1 32.0 1									
32.0									
Reviewe	ed By: f	RBM		Bingen	nsultar nans Ce	entre D		Lo	gged By: YXM
Method Notes:	: Hollow	/ Stem Auguring/Split Spoon		Kitche N	ener, Or I2B 3X9) 743-6	itario		Sh	eet: 1 of 1

Project: Hydrogeological Investigations

Location: Wilmot lands

Borehole Number: BH4

Job Number: 34896-100

Drill Date: November 30, 2010

Depth (m)	Elevation (m)	Soil Description	Symbol	Number	Type	N-Value	Standard Penetration Graph 25 50 75	Headspace (ppm)	Borehole
0.0 ft m 0.0	0.00	Ground Elevation	\sim						
		TOPSOIL	\sim						
2.0-	-0.61 0.61	SILT	\sim						
4.0	-1.52	Dark brown sandy silt with clay, light brown silty clay @ 4'dry, no staining or odour		1	SS	28			
6.0 2.0	1.52 -2.13 2.13	SILT TILL Light brown clayey silt till, some small stones, dry, no		2	SS	36			
8.0	-3.05	staining or odour Silty SAND Light brown silty sand, loose,		3	SS	23			
10.0	3.05	fine, moist to wet @8', light brown dry clay @ 9, CLAY	Ű	4	SS	21			
14.0		Grey clay, trace silt, fine grained, stiff, no staining or odour, slightly moist							
16.0				5	SS	23			
18.0 6.0 20.0 6.0	-6.10 6.10	Sandy SILT Grey sandy silt, fine grained,		6	SS	49			
22.0	-7.62 7.62	saturated, no staining or odour							
26.0	-8.23 8.23	CLAY Grey clay, fine grained, stiff, no staining or odour, dry	Ű	7	SS	47	I		
28.0									
32.0									
34.0									
Reviewe	ed By: F	RBM			nsultar			Lo	gged By: YXM
Method: Notes:	: Hollow	v Stem Auguring/Split Spoon	520	Kitche N	nans Ce ener, Or 2B 3X9) 743-6	itario	IIVE		eet: 1 of 1

Project: Hydrogeological Investigations

Location: Wilmot lands

Borehole Number: BH5

Job Number: 34896-100

Depth (m)	Elevation (m)	Soil Description	Symbol	Number	Type	N-Value	Standard Penetration Graph 25 50 75	Headspace (ppm)	Borehole
0.0 ft m 0.0	0.00 0.00	Ground Elevation TOPSOIL	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~						
2.0	-0.61 0.61	Clayey SILT	\sim						
2.0 4.0 6.0 2.0	-1.52	Grey to light brown silt and clay, fine grained, soft, moist, no staining or odour	T	1	SS	27			
-	1.52	Silty CLAY Light grey to grey silty clay, trace sand, fine grained, stiff, silty wet sand seam @ 21',	H	2	SS	35			
8.0		damp to moist, no staining or odour		3	SS	74			
2.0			H	4	SS	32			
4.0			H						
			H	5	SS	24			
8.0 6.0			H H	6					
2.0 4.0			H	6	SS	24			
6.0 4 8.0	-7.62 7.62 -8.23 8.23	CLAY TILL Grey silty clay till, trace sand, trace stone, stiff, moist to		7	SS	93			
8.0		\slight moist/							
2.0									
4.0									
		RBM / Stem Auguring/Split Spoon		Bingen Kitche N	n sultar nans Ce ener, Or I2B 3X9	entre D Itario			gged By: YXM
Notes:) 743-6			Sh	eet: 1 of 1

Project: Hydrogeological Investigations

Location: Wilmot lands

Borehole Number: BH6

Job Number: 34896-100

Depth (m)	Elevation (m)	Soil Description	Symbol	Number	Type	N-Value	Standard Penetration Graph 25 50 75	Headspace (ppm)	Borehole
0.0 ft m 0.0	0.00 0.00	Ground Elevation TOPSOIL	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~						
2.0			1,11,1						
4.0	-1.22 1.22	Silty CLAY	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	1	ss	16	1		
6.0 2.0		Light brown silty clay, little sand, moist to very moist, no staining or odour	H	2	SS	14			
8.0	-2.44 2.44	Silty SAND		3	SS	29			
10.0	-3.05 3.05	Light brown silty sand, some clay, wet					$\mathbf{\Lambda}$		
12.0		Silty CLAY Light grey silty clay, dry		4	SS	70	7		
14.0 14.0	-4.57	Silty SAND Light brown silty sand, little clay, trace stone, slight wet Silty CLAY							
16.0 H	4.57	Greyish brown silty clay, some sand,fine grained, stiff slightly moist	Ŧ	5	SS	50			
18.0 20.0	-5.49 5.49	Silty SAND Lihgt grey clayey silty sand, fine grained, slightly wet to saturated							
22.0		Silty CLAY Grey silty clay, some sand, fine grained, stiff, moist CLAY TILL		6	SS	65			
24.0		Grey sandy silty clay till, some stones, fien grained, stiff, damp to moist							
26.0 4 8.0				7	SS	65			
30.0									
32.0	-9.75 9.75		4	8	SS	75			
34.0 + 10.0	240.404.0								
 Reviewe Method Notes:	-	RBM v Stem Auguring/Split Spoon		Bingen Kitche N	nsultar nans Ce ener, Or I2B 3X9) 743-6	entre D Itario			gged By: YXM eet: 1 of 1
			_	(519) 743-6	500		Sn	

Project: Hydrogeological Investigations

Location: Wilmot lands

Borehole Number: BH7

Job Number: 34896-100

Depth (m)	Elevation (m)	Soil Description	Symbol	Number	Type	N-Value	Standard Penetration Graph	Headspace (ppm)	Borehole
0.0 <u>ft m</u> 0.0	0.00 0.00	Ground Elevation TOPSOIL	~ (
2.0	-0.76		\sim						
, o uhuhuhu	0.76	Silty CLAY Light brown silty clay, little sand, stiff, damp to moist, no staining or odour	H	1	SS	52			
.0 + 2.0			H	2	SS	57			
0. 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			Ħ	3	SS	52			
	-3.66		H	4	SS	46	$\langle \langle \langle \rangle \rangle$		
	3.66	SILT TILL Light brown to grey clayey silt till, some sand, some small stones, fine grained, some							
		pebbles @ 16', dry		5	SS	71			
.0 1 1 .0 1 .0 1 .0 1			000						
			0000	6	ss	92			
0 Internet			-						
5.0 1 - 8.0	-8.23 8.23			7	SS	50			
Review				Bingen	onsultar nans Ce	entre D		Lo	gged By: YXM
Method Notes:	: Hollov	v Stem Auguring/Split Spoon		N	ener, Or 12B 3X9 1) 743-6)		Sh	eet: 1 of 1

Project: Hydrogeological Investigations

Location: Wilmot lands

Borehole Number: BH8

Job Number: 34896-100

Depth (m)	Elevation (m)	Soil Description	Symbol	Number	Type	N-Value	Standard Penetration Graph 25 50 75	Headspace (ppm)	Borehole
0.0 <u>ft m</u> 0.0 2.0 <u></u>	0.00 0.00 -0.76	Ground Elevation TOPSOIL	2222						
4.0	0.76	Silty CLAY Light brown silty clay, trace sand, stiff, dry,gravelly sand	H	1	ss	30			
6.0 2.0		with stones @ 16' no staining or odour		2	ss	55			
8.0 1 1 1			H	3	SS	35			
10.0 - + 			H H H						
16.0 18.0 18.0 18.0 10 10 10 10 10 10 10 10 10 10 10 10 10	-4.88 4.88	SILT TILL Grey silt till, very stiff, dry, no staining or odour, light brown moist to wet silty sand @ 22'.		4	SS	125			
22.0				5	SS	50			
26.0 4 8.0	-7.62 7.62 -8.23 8.23	SAND Light brown sand, fine grained, stiff, saturated, moist silty clay		6	SS	99			
28.0 H	8,23	@ 27', no staining or odour							
30.0 32.0 11 10.0									
34.0 Reviewe Method Notes:	-	RBM v Stem Auguring/Split Spoon		Bingen Kitche N	onsultar nans Ce ener, Or I2B 3X9	entre D ntario			gged By: YXM eet: 1 of 1

Project: Hydrogeological Investigations

Location: Wilmot lands

Borehole Number: BH9

Job Number: 34896-100

Depth (m)	Elevation (m)	Soil Description	Symbol	Number	Type	N-Value	Standard Penetration Graph 25 50 75	Headspace (ppm)	Borehole	
0.0 <u>ft m</u> 0.0	0.00 0.00	Ground Elevation TOPSOIL	~~							
2.0			22/2							
4.0	-1.07 1.07	Sandy SILT Light brown sandy silt with		1	SS	25	i			
2.0 4.0 6.0 2.0	-2.29	clay, some stones, moist, no staining or odour		2	SS	18				
8.0	2.29	Silty CLAY Grey silty clay, trace sand,	Æ	3	SS	27				
10.0-		soft, slightly moist, no staining or odour, water coming out @ 13'	Ŧ	4	SS	25				
12.0-			Ŧ							
14.0	-4.57 4.57		Ŧ							
16.0	4.57	CLAY Grey clay, soft, fine grained, slightly moist, no staining or		5	SS	30				
18.0		odour								
22.0-				6	SS	39				
24.0										
26.0	-8.23		Ű	7	SS	42				
28.0	8.23									
30.0										
32.0										
34.0										
	Reviewed By: RBM			MTE Consultants Inc. 520 Bingemans Centre Drive				Logged By: YXM		
Method: Notes:	Hollow	v Stem Auguring/Split Spoon		Kitche N	ener, Or 12B 3X9) 743-6	ntario)		Sh	eet: 1 of 1	

Project: Hydrogeological Investigations

Location: Wilmot lands

Borehole Number: BH10

Job Number: 34896-100

Depth (m)	Elevation (m)	Soil Description	Symbol	Number	Type	N-Value	Standard Penetration Graph	Headspace (ppm)	Borehole
0.0 ft m 0.0	0.00	Ground Elevation TOPSOIL	{						
2.0	-0.76								
4.0	0.70	Clayey SILT Light brown clayey silt, trace sand, fine grained, stiff, dry, no staining or odour	H	1	SS	34			
0.0 ft m 0.0 2.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4				2	SS	64			
8.0	<u>-2.74</u> 2.74	Silty SAND	K	3	SS	54			
10.0		Grey silty sand, fine grained, moist to wet, no staining or odour		4	SS	67			
14.0									
16.0-	-4.57 4.57	CLAY Grey clay, trace sand, soft, dry, no staining or odour		5	SS	33	{		
4.0 14.0 16.0 18.0 20.0 4 6.0		dry, no stanning of oddar					\mathbf{A}		
1				6	SS	53)		
22.0									
26.0 - 8.0	-8.23 8.23			7	SS	41			
30.0									
32.0									
34.0									
Reviewe	ed By: I	RBM			nsultar nans Ce			Lo	gged By: YXM
Method: Notes:	Hollow	/ Stem Auguring/Split Spoon	520	Kitche	inaris Ce ener, Or I2B 3X9) 743-6	itario			eet: 1 of 1

Project: Hydrogeological Investigations

Location: Wilmot lands

Borehole Number: BH11

Job Number: 34896-100

Depth (m)	Elevation (m)	Soil Description	Symbol	Number	Type	N-Value	Standard Penetration Graph 25 50 75	Headspace (ppm)	Borehole
0.0 ^{ft} m 0.0 2.0	0.00	Ground Elevation TOPSOIL	$\langle l_{l} \rangle$						
4.0-1-1	0.76	CLAY TILL Light brown silty clay till with sand, stiff, dense, fine grained, dry, no staining or odour		1	SS	64			
6.0 + 2.0				2	SS	50			
8.0		14		3	SS	41			
12.0				4	SS	41			
14.0	-4.57 4.57								
16.0		Silty CLAY Grey silt with some silt and sand, dense, fine grained, slightly moist to moist, no staining or odour	H H H	5	SS	20			
22.0			HHH	6	SS	38			
26.0 - 8.0	-7.62 7.62 -8.23 8.23	Clayey SILT Grey clayey silt with sand, stiff, fine grained, dry, no staining	1	7	SS	85			
28.0 30.0 32.0 32.0 34.0 10.0 34.0 10.0	8.23	or odour							
Reviewe Method:		RBM / Stem Auguring/Split Spoon		Bingen Kitche	nsultar nans Ce ener, Or	entre D Itario		Lo	gged By: YXM
Notes:		0,		N	12B 3X9) 743-6			Sh	eet: 1 of 1

Project: Hydrogeological Investigations

Location: Wilmot lands

Borehole Number: BH12

Job Number: 34896-100

Depth (m)	Elevation (m)	Soil Description	Symbol	Number	Type	N-Value	Standard Penetration Graph 25 50 75	Headspace (ppm)	Borehole
0.0 ft m 0.0	0.00 0.00	Ground Elevation TOPSOIL	22						
	-0.76 0.76	CLAY TILL Light brown silty clay till with sand, stiff, fine grained, dry, no staining or odour		1	SS	38			
6.0 - 2.0	-1.98 1.98	Sandy SILT		2	SS	37			
8.0	-2.74 2.74	Light brown sandy silt, trace clay, dry,moist to wet @ 8', no staining or odour	F	3	SS	53			
12.0-1		Silty CLAY Light brown silty clay, moist to wet, no staining or odour		4	SS	35			
4.0		Silty SAND Grey silty sand with clay, fine grained, loose, moist, wet to saturated @ 16', no staining or odour							
				5	SS	52			
8.0 + + + + + + + + + + + + + + + + + + +	-6.40			6		45			
2.0	6.40	Silty CLAY Grey silty clay, stiff, dense, fine grained, slightly moist, no staining or odour	H		SS	40			
6.0 8.0	-8.23 8.23		H	7	SS	56			
	0.23								
A.0	ad But	BM	N		onsulta	nts Inc			
		v Stem Auguring/Split Spoon	520	Kitche N	nans Ce ener, Or I2B 3X9) 743-6	ntario)	rive		gged By: YXM eet: 1 of 1

Project: Hydrogeological Investigations

Location: Wilmot Lands

Test Trench Number: TT1

Job Number: 34896-100

Depth (m)	Elevation (m)	Soil Description	Symbol	Number	Type	Headspace (ppm)	Comments
0.0 ft m 	0.00	Ground Elevation TOPSOIL Dark brown topsoil, rootlets, wood p soft, damp					
4.0	-0.76 0.76	Silty CLAY Brown silty clay, sand seam @ 3-3.8 soft, sticky, moist to very moist	2				No seepage observed during excavation Caving @ 3 feet
5.0							
			# # # #		14		
	<u>-3.20</u> 3.20						
Reviewo Method Notes:			MTE Consultant 520 Bingemans Cen Kitchener, Onta N2B 3X9 (519) 743-650	tre Driv ario	e		Logged By: YXM Sheet: 1 of 1

Project: Hydrogeological Investigations

Location: Wilmot Lands

Test Trench Number: TT2

Job Number: 34896-100

Depth (m)	Elevation (m)	Soil Description	Symbol	Number	Type	Headspace (ppm)	Comments
0.0 ft m 	0.00	Ground Elevation TOPSOIL Dark brown topsoil, rootlets of corn, soft, damp					
	-1.37	Clayey SILT Brown silt and clay, some sand, damp to very moist,soft, no staining or odour					No seepage observed during excavation
5.0	1.37	Silty CLAY Brown silty clay, little sand, sticky, moist, no staining or odour	+++++++++				
	-2.44 2.44 -3.35	Sandy SILT Grey sandy silt, clayey, fine grained, moist to slight wet					
	3.35						14.
Reviewe Method		0e 520 Bingen Kitche	onsultant nans Cen ener, Onta 12B 3X9	tre Drive	9		Logged By: YXM
Notes:		(519) 743-65(00			Sheet: 1 of 1

Project: Hydrogeological Investigations

Location: Wilmot Lands

Test Trench Number: TT3

Job Number: 34896-100

Depth (m)	Elevation (m)	Soil Description	Symbol	Number	Type	Headspace (ppm)	Comments
0.0 ft m - - - - - - - - -	0.00 0.00 -0.46 0.46	Ground Elevation TOPSOIL Dark brown topsoil, rootlets of corn, soft, damp					
2.0		SILT Brown ssandy clayey silt, loose, damp, no staining or odour					No seepage observed during excavation
4.0	<u>-1.07</u> 1.07	Silty CLAY Brown to dark brown silty clay, little sand, hard, moist to damp, no staining or odour	H H H				
6.0			H+++++				
'	-3.35 3.35		H H				
2.0 Reviewe Method Notes:		0e 520 Bingen Nitche	onsultant nans Cen ener, Onta I2B 3X9 I) 743-650	tre Driv ario	e		Logged By: YXM Sheet: 1 of 1

Project: Hydrogeological Investigations

Location: Wilmot Lands

Test Trench Number: TT4

Job Number: 34896-100

Depth (m)	Elevation (m)	Soil Description	Symbol	Number	Type	Headspace (ppm)	Comments
0.0 + 0.0	0.00 0.00 -0.46 0.46	Ground Elevation TOPSOIL Dark brown topsoil, rootlets, soft, damp	$l_{l_l} l_{l_l} l_{l_l}$				
4.0	0.46	Silty CLAY Brown silty clay, little sand, damp to moist, changing to grey below 8' and damp to dry with trace sand, no staining or odour	#/#/#/#/#/#/				No seepage observed during excavation
6.0 2.0 2.0 8.0			+++++++++++++++++++++++++++++++++++++++				
	-3.35 3.35		# # # #				
2.0-	1						
Reviewe Method Notes:		0e 520 Bingen Nitche N	nsultant nans Cen ener, Onta I2B 3X9) 743-650	tre Drive ario	ə		Logged By: YXM Sheet: 1 of 1

Project: Hydrogeological Investigations

Location: Wilmot Lands

Test Trench Number: TT5

Job Number: 34896-100

Depth (m)	Elevation (m)	Soil Description	Symbol	Number	Type	Headspace (ppm)	Comments
.0 <u>ft m</u> 0.0	0.00	Ground Elevation	\sim				
		TOPSOIL Dark brown topsoil, rootlets, soft, damp	1/1/1/1				
0	-0.46 0.46	Sandy SILT Brown to dark brown sandy clayey silt, few big stones @ 2-2.5', trace gry sand @ 2.5', no staining or odour					No seepage observed during excavation
	-0.91 0.91	Silty CLAY Brown to dark brown silty clay, trace sand, hard, sticky, damp, no staining or odour	HH.				
			HHH H				
0 - 2.0 - - - -			TH H				
- 1 0 - 1 1 - 1 - 1			H/H/H				
	-3.20 3.20		F/H/H	1			
- - - - - - - -							
Reviewo Method		oe Singer Kitch	ener, Onta N2B 3X9	tre Driv ario	e		Logged By: YXM
Notes:		(519	9) 743-650	00			Sheet: 1 of 1

Project: Hydrogeological Investigations

Location: Wilmot Lands

Test Trench Number: TT6

Job Number: 34896-100

Depth (m)	Elevation (m)	Soil Description	Symbol	Number	Type	Headspace (ppm)	Comments
0.0 + + + + + + + + + + + + + + + + + +	0.00	Ground Elevation TOPSOIL Dark brown topsoil, rootlets, soft, damp	$\{\lambda_l,\lambda_l,\lambda_l\}$				
2.0	-0.46 0.46	Silty CLAY Brown silty clay, trace sand, sticky, trace stones @ 4'and getting hard and dry below 4', more stones and clayey @ 7', no staining or odour	井井井井井				No seepage observed during excavation
6.0 2.0 8.0 			+++++++++++++++++++++++++++++++++++++++				
- - - - - - - - - - - - - - - - - - -	-3.05 3.05		H/H/F				
- - - - - - 2.0 -							
Reviewe Method: Notes:		De 520 Bingen Nitche N	n sultant nans Cen ener, Onta I2B 3X9) 743-650	tre Drive ario	e		Logged By: YXM Sheet: 1 of 1

Project: Hydrogeological Investigations

Location: Wilmot Lands

Test Trench Number: TT7

Job Number: 34896-100

Depth (m)	Elevation (m)	Soil Description	Symbol	Number	Type	Headspace (ppm)	Comments
0.0 <u>ft m</u> 0.0 - - - - - - - - - - - -	0.00	Ground Elevation TOPSOIL Dark brown topsoil, rootlets, soft, damp					
	-0.61	Sandy SILT Brown sandy clayey silt, gravelly, loose, dry to moist, no staining or odour					
4.0	-1.68 1.68	Silty CLAY Brown to dark brown silty clay, hard, sticky, damp to moist, no staining or odour	HHH				
6.0	-2.13 2.13	SAND AND GRAVEL Brown sand and gravel, some clay, saturated, no staining or odour Silty CLAY					Seepage observed during excavation @6'
8.0 - - - - - - - - - - - - - - - - - -	-3.20	Brown silty clay, gravelly, moist, no staining or odour	+++++++++++++++++++++++++++++++++++++++				
	3.20						
Review Method Notes:		0e S20 Bingen Nitche	nans Cen ener, Onta 2B 3X9) 743-650	itre Drivo ario	e		Logged By: YXM Sheet: 1 of 1

Project: Hydrogeological Investigations

Location: Wilmot Lands

Test Trench Number: TT8

Job Number: 34896-100

Depth (m)	Elevation (m)	Soil Description	Symbol	Number	Type	Headspace (ppm)	Comments
0.0 ft m - - - -	0.00	Ground Elevation TOPSOIL Dark brown topsoil, rootlets, soft, damp	12121				
	-0.46	Silty CLAY	12/1				
		Brown silty clay, little sand, stones @ and below 6' (few big boulders), damp to little moist, no staining or odour moist, getting dry and hard below 4', more stones @ 7', more clayey and sticky below 7', no staining or odour	#/#/#/#				No seepage observed during excavation
4.0			并并并				
- - - - - - - - - - - - - - - - - - -	2.50		#/#/#/#				
- - - - - - - - - - - - - - - - - - -	-2.59 2.59	Grey to dark grey silty clay, hard, damp	HHHH				
- - - - - 2.0-	-3.20 3.20		+				
Reviewe Method		0e 520 Binger	onsultant nans Cen ener, Onta 12B 3X9	tre Drive	e		Logged By: YXM
Notes:) 743-65(00			Sheet: 1 of 1

Project: Hydrogeological Investigations

Location: Wilmot Lands

Test Trench Number: TT9

Job Number: 34896-100

Date: December 21, 2010

Depth (m)	Elevation (m)	Soil Description	Symbol	Number	Type	Headspace (ppm)	Comments
0.0 <u>ft m</u> 0.0 - - - - - -	0.00	Ground Elevation TOPSOIL Dark brown topsoil, rootlets, soft, damp	$\left \left \left$				
2.0	0.46 -0.91 0.91	Sandy SILT Brown sandy silt, clayey, fine grained, loose, damp, no staining or odour Silty CLAY					No seepage observed during excavation
4.0		Brown silty clay, little sand, soft, damp to slight moist	H/H/H				
6.0 - 2.0			HHH H				
- - - - - 8.0 - - - - - - - - -			H/H/H				
0.0			HHHH				
	-3.35 3.35		TT-				
Reviewe Method: Notes:		oe S20 Bingen Nitche	n suitant nans Cen ener, Onta 2B 3X9) 743-650	tre Drive ario	9		Logged By: YXM Sheet: 1 of 1

Project: Hydrogeological Investigations

Location: Wilmot Lands

Test Trench Number: TT10

Job Number: 34896-100

Date: December 21, 2010

Depth (m)	Elevation (m)	Soil Description	Symbol	Number	Type	Headspace (ppm)	Comments
0.0 ft m - - - - - - - - - - - - - - - - - - -	0.00 0.00 -0.46 0.46	Ground Elevation TOPSOIL Dark brown topsoil, rootlets, soft, damp Clayey SILT Brown clayey silt, some sand, loose, fine	121221				
2.0	-1.22	Brown clayey silt, some sand, loose, fine grained,moist to wet, no staining or odour	1.				Seepage observed during excavation @ 3.5'
6.0		Silty CLAY Brown silty clay, little sand, soft, moist, no staining or odour	#(#(#)#)				
			#\#\#\#\				
- - - - - - - - - - - - - - - - - - -	-3.20 3.20		H H				
Review Method Notes:		oe Sitten Kitche	onsultant nans Cer ener, Ont V2B 3X9 9) 743-650	ntre Driv ario	e		Logged By: YXM Sheet: 1 of 1

Project: Hydrogeological Investigations

Location: Wilmot Lands

Test Trench Number: TT11

Job Number: 34896-100

Date: December 21, 2010

Depth (m)	Elevation (m)	Soil Description	Symbol	Number	Type	Headspace (ppm)	Comments
0.0 ft m - - - - - - -	0.00	Ground Elevation TOPSOIL Dark brown topsoil, rootlets, soft, damp	111111				
	0.46	Sandy SILT Brown sandy silt, clayey, fine grained, loose, moist, no staining or odour					No seepage observed during excavation
4.0 — - - - - - - - - - - - - - - - - - - -	-1.22 1.22 -2.13 2.13	SILT AND CLAY Brown silt and clay, some sand, very moist, no staining or odour	世世世世				
8.0 - - - - - - - - - - - - - - - - - - -		Clayey SILT Grey clayey sandy silt, fine grained, loose, slight wet, no staining or odour					
	-3.35 3.35						
Review Method		0e 520 Binger Nitche	ener, Onta N2B 3X9	itre Driv ario	e		Logged By: YXM
Notes:		(519	9) 743-650	00			Sheet: 1 of 1

Project: Hydrogeological Investigations

Location: Wilmot Lands

Mini-Piezometer: MP1-11

Job Number: 34896-100

Drill Date: January 11, 2011

	Elevation (m)	Soil Description	Symbol	Number	Type	Recovery (%)	Headspace (ppm)	Groundwater Observations and Well Details
-4.0 ft m -4.0 ft m	0.00 0.00 0.15 0.30 0.91 0.91			sultant	s Inc.			Sand Pack Bentonite
Nethod: H		520) Bingema Kitchen N2i	ns Cen	tre Drive ario	9		Logged By: YXM Sheet: 1 of 1

Project: Hydrogeological Investigations

Location: Wilmot Lands

Mini-Piezometer: MP2-11

Job Number: 34896-100

Drill Date: January 11, 2011

Depth (m)	Elevation (m)	Soil Description	Symbol	Number	Type	Recovery (%)	Headspace (ppm)	Groundwater Observations and Well Details
ft m -4.0- 	0.00 0.00 -0.15 0.15 -0.61 -0.84 0.84	Ground Elevation TOPSOIL Silty CLAY Greyish brown silty clay, little to trace sand, very moist Clayey SILT Greyish brown clayey silt, some sand, moist to wet Silty CLAY Grey silty clay, hard, moist	2 2 2 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4					Sand Pack Bentonite
Reviewe Method: Notes:			Bingema Kitchene N2I	ns Cen	tre Drive ario	•		Logged By: YXM Sheet: 1 of 1

Project: Hydrogeological Investigations

Location: Wilmot Lands

Mini-Piezometer: MP3-11

Job Number: 34896-100

Drill Date: January 11, 2011

Depth (m)	Elevation (m)	Soil Description	Symbol	Number	Туре	Recovery (%)	Headspace (ppm)	Groundwater Observations and Well Details
ft m -4.0	0.00 0.00 -0.15 0.15	Ground Elevation TOPSOIL Clayey SILT	223					Bentonite Stick-Up
2.0	-1.07	Dark grey clayey silt, some sand, wet Sandy SILT Brown sandy silt, some clay, moist to wet Silty CLAY Brown silty cly, some sand, trace stone, moist Silty SAND	# # # # # #					Slot Screen
Reviewe Method Notes:				ns Cen	tre Drive ario	3		Logged By: YXM Sheet: 1 of 1

LOC	JECT Proposed Development - Wilmot Em ATION New Hamburg, Ontario ING METHOD Continuous Flight Hollow Ste						T	SHEA				arch 13,	ı —		engi Teci	REF. INEE HNIC			oghrin
DEPTH ELEV netres	DESCRIPTION	STRAT PLOT		NUMBER	SAM	PLES	ELEVATION SCALE	+FIE ▲PO	LD VAN CKET P	E ∆TO ENETR 00 1	RVANE OMETE 50 2		W _P	ATURAL DISTURE DNTENT W 		QUID LIMIT ₩L →	UNIT WEIGHT		GROUND WATEF OBSERVATIONS AND REMARKS GRAIN SI
	SURFACE ELEVATION TOPSOIL: Dark brown clayey silt, frozen	л ГП	T	1	SS	-	ELE					30		0 30			kN/m ³		GRAIN SI DISTRIBUTIO GR SA Stickup Well Pro
	CLAYEY SILT: Very stiff brown clayey silt, trace sand, DTPL					8	_												Set in Concrete 50 mm Plastic R
		ľ		2	SS	19													
			\parallel	3	SS	25													
		Í		4	SS	28							ŀ						
<u>3.</u> 0_	becoming stiff, grey, APL			5	SS	9	_	₊											
			$\left \right $																
		Í																	Bentonite Seal
			1	6	SS	10		•											
<u>6.1</u> _	becoming very stiff, occasional silt layers, wet			7	SS	21													
			1																
				8	55	18													
		P	1	0	55	10	_												
																			Filter Sand
		K		9	SS	18													• • •
			$\left \right $																Slotted Screen
11 1		[10	SS	23	-											·日·	
<u>11.1</u>	BOREHOLE TERMINATED AT 11.1 m																	W/otr	er Level Readings:
																			l: 10.6 m

	IECT Proposed Development - Wilmot Em ATION New Hamburg, Ontario NG METHOD Continuous Flight Hollow Ste	-			s			E	BORIN	G DAT	Έ Ma	arch 14,	2018		PML ENGI TECH	INEE			oghrin
	SOIL PROFILE			5	SAM	PLES	Щ	SHEAR	STREN	IGTH	(kPa)	0.0		no N/	Luz		_		
DEPTH ELEV metres	DESCRIPTION SURFACE ELEVATION	STRAT PLOT	NIIMDED	NUMBER	түре	"N" VALUES	ELEVATION SCALE	+FIELD ▲POCK 50 DYNAMIC STANDA 20	100) 15 E PEN NETR/	ETRAT	ION ×	W _P W		ENT (%				GROUND WATER OBSERVATIONS AND REMARKS GRAIN SIZ DISTRIBUTION GR SA SI
0.33	TOPSOIL: Dark brown clayey silt topsoil,	\sim	Ţ			-													Stickup Well Prote
0.33	frozen CLAYEY SILT: Firm brown clayey silt, some sand, APL			+	SS	6													Set in Concrete 50 mm Plastic Ris
		И		2	SS	4		$\left \right\rangle$											
<u>1.5</u>	becoming stiff, layered with brown silt, some fine sand, wet	4		3	SS	14													
			4	4	SS	25			•				•						
<u>3.0</u>	becoming grey clayey silt, trace sand, DTPL, occasional sand partings		ŧ	5	SS	13													Bentonite Seal
			6	6	GS														
				7	SS	13								*					
				2	SS	11													Filter Sand
						2													Slotted Screen
8.1	BOREHOLE TERMINATED AT 8.1 m			•	SS	22												<u>∵H</u> . Wati	er Level Readings:
																		Initia	l: Dry
NOTE	<u> </u>																		

Peto MacCallum Ltd.

LO	OJECT Proposed Development - Wilmot En CATION New Hamburg, Ontario RING METHOD Continuous Flight Hollow St			ands				BORII	IG DA1	r e Ma	arch 14,	2018		E	ML RE NGINE ECHN			oghrin
	SOIL PROFILE	0		SAN	IPLES	щ	SHEA	R STRE	NGTH	(kPa)			NIA					
DEPT ELE (metre	DESCRIPTION	STRAT PLOT	NUMBER	ТҮРЕ	"N" VALUES	ELEVATION SCALE	A POC 5 DYNAI STANE	/IIC COI		JMETE 50 20 IETRAT ATION	ROQ 00 10N × TEST●	W _P		TURAL ISTURE NTENT W 				GROUND WATER OBSERVATIONS AND REMARKS GRAIN SIZ DISTRIBUTION GR SA SI
0.2	SURFACE ELEVATION TOPSOIL: Dark brown clayey silt, frozen		~	_			2	0 4	06	а 0	30	1	0 20	30	40	kN/m		GR SA SI
	CLAYEY SILT: Firm brown clayey silt, trace	\prod		SS	6													Set in Concrete
0.76	SANDY SILT: Loose brown sandy silt, trace clay, moist		2	SS	8													50 mm Plastic Ris
<u> 1.5</u>	becoming compact, occasional clayey		3	SS	11													
				_														
			• 4	SS	16													
3.0	CLAYEY SILT: Stiff grey clayey silt, trace	[· :																Bentonite Seal
	sand, APL		5	SS	14		•											
			6	GS						Ť								
		Í																
			7	SS	12													
		И																
			1—	_														Filter Sand
			8	SS	13		I											•
																		Slotted Screen
		И																•
			9	SS	12												·	<u>.</u>
8.1	BOREHOLE TERMINATED AT 8.1 m		f 															er Level Readings:
																	Initia	l: Dry

DEPTH ELEV metres) 0.25 TOP	IETHOD Continuous Flight Hollow Ste SOIL PROFILE DESCRIPTION		jers	SAM								2018		ENGIN				ghrin
ELEV metres) 0.25 TOP CLA' sand		LOT		SAM					NOTU	<u></u>				TECHI	VICIAI	ND.	. Bric	ж
0.25 TOP CLA sand		STRAT PLOT	NUMBER	TYPE	PLES Sannar	ELEVATION SCALE	+FIE APO DYNA STAN	MIC CO DARD P	E △TOF ENETR()0 1! NE PEN ENETR	RVANE DMETER	ION ×	W _P 		NT (%)	N∟ -)			GROUND WATER OBSERVATIONS AND REMARKS GRAIN SIZE DISTRIBUTION GR SA SI
	RACE ELEVATION SOIL: Dark brown clayey silt, frozen YEY SILT: Firm brown clayey silt, trace	ĨĨ	1	SS	8		•				0				KIN	I/m ³		Stickup Well Protect Set in Concrete
1.5	, noist		2	SS	13													50 mm Plastic Rise
SILT	Y SAND: Compact brown silty sand,		3	SS	12													
			4	SS	15													
<u>3.0</u> beco satur	ming grey, occasional clayey lenses, rated		5	SS	18													
			6	SS	25													Bentonite Seal
			7	SS	24													
_ <u>7.6</u> beco	oming dense		8	SS	31													
9.1																		Filter Sand
	: Compact grey silt, some fine sand, e clay, saturated, occasional clayey es		9	SS	21			Í										
																		Slotted Screen
11.1 BOR	REHOLE TERMINATED AT 11.1 m		10	SS	26			ł										
																		<u>r Level Readings:</u> 10.4 m

L		TION New Hamburg, Ontario	-	nent La		GOF	D	BOREHOL	DATE March 1		E	ML REI NGINEI	ER	18KF009 W. Loghrin	1 of
В	BORI	NG METHOD Continuous Flight Hollow Ster SOIL PROFILE	m Au	gers	SVIV	PLES		SHEAR STRENG	TH (kPa)				CIAN	D. Brice	
EL		DESCRIPTION SURFACE ELEVATION	STRAT PLOT	NUMBER	JAPE 1	"LES N.: VALUES	ELEVATION SCALE	SHEAR STRENG +FIELD VANE △ POCKET PENE 50 100 DYNAMIC CONE STANDARD PENE 20 40	TROMETER O Q 150 200	W _P		WL	-	GROUND WAT OBSERVATION AND REMARK GRAIN DISTRIBU GR SA	IS SIZE FION SI
0).36	TOPSOIL: Dark brown clayey silt, trace sand, frozen))	1	SS	5		•						Stickup Well F Set in Concret	
		CLAYEY SILT: Firm brown clayey silt, some sand, APL		2	SS	7		→						50 mm Plastic	Rise
				3	SS	6									
_ 4	<u>2.3</u>	becoming stiff, grey, no zones	- 2	4	SS	12									
				5	SS	12		•						Bentonite Seal	
4	4.5	SANDY SILT: Compact grey sandy silt, saturated, occasional clayey lenses		6	SS	16									
(6.1	CLAYEY SILT: Very stiff grey clayey silt,												Filter Sand	
		trace sand, DTPL, occasional silt lenses, wet		7	SS	17								Slotted Screer	I
8	8.1	BOREHOLE TERMINATED AT 8.1 m		8	SS	19		+						Water Level Readings	<u>.</u>
														Initial: 5.7 m	
	IOTE														

	IECT Proposed Development - Wilmot Em ITION New Hamburg, Ontario NG METHOD Continuous Flight Solid Ster			nds			BOF	ING DATE	March 14,	2018	PML F ENGIN TECH	IEER	18KF0 W. Lo D. Brid	ghrin
DON	SOIL PROFILE	ii Auge	13	SAM	PLES	щ	SHEAR ST	ENGTH (kP	a)					
DEPTH ELEV netres)	DESCRIPTION SURFACE ELEVATION	STRAT PLOT	NUMBER	ТҮРЕ	"N" VALUES	ELEVATION SCALE	+FIELD VA ▲POCKET 50 DYNAMIC C STANDARD 20	100 150	200	W _P 				GROUND WATER OBSERVATIONS AND REMARKS GRAIN SIZ DISTRIBUTION GR SA SI
0.25	TOPSOIL: Dark brown clayey silt, trace sand, frozen	ĥĩ	1	SS				ŤŤ	Ť			KIWIII		Stickup Well Prote
	CLAYEY SILT: Very stiff brown clayey silt, trace sand, DTPL		2	SS										50 mm Plastic Ris
		H												
			3	SS										
		K	4	SS										Bentonite Seal
			5	SS		-								
<u>4.5</u>	becoming firm, grey, occasional silt layers, wet		6	SS		-								Filter Sand
														Slotted Screen
6.1														
	SILT: Compact grey silt, some sand, trace clay, wet, occasional clayey layers BOREHOLE TERMINATED AT 6.5 m		7	SS										· · · · · · ·
	BOREHOLE TERIVIINATED AT 6.5 m													<u>r Level Readings:</u> ∶4.5 m
NOTE														

Peto MacCallum Ltd.

						G OF	ים				110	. 10	1				_		1 of
	DECT Proposed Development - Wilmot Emp ATION New Hamburg, Ontario	oloyn	nent	t Lan	lds				BORII	NG DA	re Ma	ırch 13,	2018			. REF SINEE		18KF(W. Lo	
BOF	Continuous Flight Hollow Ste	m Au	iger				<u> </u>	SHEAF			(kDa)				TEC	HNIC	IAN	D. Bri	ce
<u>DEPT</u> ELEV metre	DESCRIPTION	STRAT PLOT		NUMBER	SAM	PLES	ELEVATION SCALE	+FIEL ▲POC 5	D VAN KET PI 0 1 MIC CO ARD P	E △TOI ENETR 00 1 NE PEN ENETR	(KPa) RVANE DMETEI 50 20 LETRAT ATION 1 60 8	ION ×	W _P	CC	I ENT (W UNIT WEIGHT		GROUND WATER OBSERVATIONS AND REMARKS GRAIN SIZI DISTRIBUTION GR SA SI
0.27	TODOOIL Deals have a law with the set	, Yiii		1	SS	8		•	-										Stickup Well Prote
	CLAYEY SILT: Firm brown clayey silt, some sand, APL			2	SS	7	-												50 mm Plastic Rise
<u>1.5</u>		1																	
2.3	becoming stiff, layered with brown silt, some sand, trace clay, moist			3	SS	9													
2.5	becoming very stiff/compact	ŦĦ		4	SS	28			•										
			-	5	SS	25			ļ										Bentonite Seal
		1																	
				6	SS	14	_												
<u>6.0</u>	becoming very stiff, occasional silt layers			7	SS	16													Filter Sand
		$\left \right $																	Slotted Screen
<u>7.6</u>	becoming stiff		-	8	SS	9												<u>:</u>]:	
8.1	BOREHOLE TERMINATED AT 8.1 m																		r Level Readings: 7.4 m
	ES																		

LC	DCA	ECT Proposed Development - Wilmot Em TION New Hamburg, Ontario IG METHOD Continuous Flight Hollow Ste			nt Lar		g of	B	ORI			NO те ма				E	ML RE NGINE ECHN	ER	1 of 18KF009 W. Loghrin D. Brice
		SOIL PROFILE		Ť		SAM	PLES	Ц	SHEA			(kPa)	0.00		NAT				
<u>DEP</u> ELE (metr	EV	DESCRIPTION	STRAT PLOT		NUMBER	ТҮРЕ	"N" VALUES	ELEVATION SCALE		50 1	00 1	RVANE OMETEI 50 20 LETRAT	00	W _P		N 0	LIQU LIM W T (%)	- E	GROUND WATER OBSERVATIONS AND REMARKS GRAIN SIZE DISTRIBUTION GR SA SI
0.2		SURFACE ELEVATION TOPSOIL: Dark brown clayey silt, trace		~				Ξ	:	20 4	ο e	80 8 	0	10	20	30	40	kN/m	3 GR SA SI
-	ľ	sand, frozen CLAYEY SILT: Stiff brown clayey silt, trace			1	SS	10												
	1	sand, DTPL		\mid	2	SS	11												
1.	.5		K						$ \rangle$										
		becoming very stiff, occasional silty sand layers			3	SS	16												
2.	.3	SILT: Compact grey silt, some sand, trace		4															
		clay, wet			4	SS	14												
-					5	SS	10												
<u>- 3.</u>	0	CLAYEY SILT: Stiff grey clayey silt, trace		+	-														
	:	sand, APL																	
			\mathbb{W}	1															
					6	SS	10		•										
				X															
			1																
				┟	7	SS	15												
			И	1															
_ 7.	.6	becoming APL, numerous silt layers, wet		4															Sampler wet from 7.6 m to
-	ľ				8	SS	13		†										completion
				1															
-																			
					9	SS	17												
-			И																
			\mathbb{W}	1															
11		BOREHOLE TERMINATED AT 11.1 m		4	10	SS	14		•							_	+		Upon completion of augeri
																			Open No free water
	OTES	S					1	1											

	IECT Proposed Development - Wilmot Em ATION New Hamburg, Ontario NG METHOD Continuous Flight Hollow Ste		nent La		G OF				DLE		. 10	9	E	ML REF NGINEE ECHNIC	R	1 of 18KF009 W. Loghrin D. Brice
	SOIL PROFILE		1	SAM	PLES	щ	SHEA	R STRE	NGTH	(kPa)						
DEPTH ELEV (metres	DESCRIPTION SURFACE ELEVATION	STRAT PLOT	NUMBER	TYPE	"N" VALUES	ELEVATION SCALE	UYNA STANI	50 1 VIC CO DARD P	00 1 NE PEN ENETR	RVANE OMETER 50 20 JETRAT ATION 1 60 8	ION ×	W _P WA	w ∽─── ONTEN	W _L T (%)	N/m WEIGHT	GROUND WATER OBSERVATIONS AND REMARKS GRAIN SIZE DISTRIBUTION GR SA SI
0.21	TOPSOIL: Dark brown clayey silt, some sand, frozen	ĥň	1	SS	9		•									
	CLAYEY SILT: Firm brown clayey silt, trace sand, APL															
		H	2	SS	5											
			3	SS	4											
<u>2.3</u>							$ \rangle$									
	becoming stiff, DTPL, occasional sand seams, wet		4	SS	14											Sampler wet at 2.3 m
			5	SS	14											
		11	5	33	14											
4.5	SILTY SAND: Compact grey silty sand, trace	4	·													Sampler wet at 4.5 m
	clay, saturated		6	SS	26											
6.0			: 													
	CLAYEY SILT: Very stiff grey clayey silt, trace sand, APL		7	SS	20											
		r														
			8	SS	22			•								
<u>8.1</u>	occasional sand seams, wet	7														Sampler wet at 8.1 m
		K	9	SS	17											
			9	- 55	17											
		И														
11.1	BOREHOLE TERMINATED AT 11.1 m	μμ	10	SS	14		•						 	_		
																Upon completion of augerin Open Free water at 6.0 m
NOTE																

LOC	JECT Proposed Development - Wilmot E ATION New Hamburg, Ontario ING METHOD Continuous Flight Solid Str		ent La		G OF	_				Έ Marc			E	ML REF NGINEE ECHNIC	R	18KF009 W. Loghrin D. Brice
DEPTI ELEV	SOIL PROFILE	STRAT PLOT	NUMBER	SAM	PLES	TION SCALE	SHEAR +FIELI ▲POC 50	O VANE KET PE		VANE METER	PLAS ⁻ LIMIT W _P	TIC NA MO CO	TURAL ISTURE NTENT W	LIQUIE LIMIT WL		GROUND WATER OBSERVATIONS AND REMARKS
(metres	SURFACE ELEVATION	STRA	NUN	Ĕ	^N.	ELEVATION	DYNAM STAND 20			ETRATIC ATION TE 0 80		ATER (0 20	CONTEN		kN/m ³	GRAIN SIZE DISTRIBUTION GR SA SI
0.45	brown clayey silt, DTPL-APL CLAYEY SILT: Very stiff brown clayey silt, trace sand, trace gravel, DTPL		1	SS	10											
			2	SS	15	_										
			3	SS	21	-		,								
<u>2.9</u>	becoming grey/brown, APL		4	SS	14											
3.6																Upon completion of augeri Open No free water
					2				~							

LOC	JECT Proposed Development - Wilmot Em ATION New Hamburg, Ontario ING METHOD Continuous Flight Solid Sterr		ent La		G OF		UT NE				arch 14,				ENGI	REF. INEEI HNICI	R	18KF009 W. Loghrin D. Brice
	SOIL PROFILE	0		SAM	PLES	ш	SHEAF						N/					
DEPTI ELEV (metres)	STRAT PLOT	NUMBER	ТҮРЕ	"N" VALUES	ELEVATION SCALE	▲POC 5 DYNAN STAND	KET PI 0 1 AIC CO	ENETRO 00 1 NE PEN ENETR	OMETE 50 20 IETRAT ATION	NOQ 00 10N × TEST●	W _P	ATER	ATURAL DISTUR DISTUR DISTUR W 	ENT (%		UNIT WEIGHT	GROUND WATER OBSERVATIONS AND REMARKS GRAIN SIZE DISTRIBUTION GR SA SI
0.15	SURFACE ELEVATION TOPSOIL: Dark brown clayey silt, trace sand, frozen	Î	1	SS	9		2	0 4	06	80 8	0		0 2		40	,	kN/m ³	GR SA SI
	SILT: Loose brown silt, some sand, trace clay, moist		2	SS	6													
			3	SS	11													
2.3	CLAYEY SILT: Stiff brown clayey silt, trace sand, APL, occasional sand layers		4	SS	10													
<u>3.0</u>	becoming grey		5	SS	11													
<u>4.5</u>	becoming layered with grey silt, some sand,		6	SS	12													
	wet		0	55	12				K									
6.5	BOREHOLE TERMINATED AT 6.5 m		7	SS	10													Upon completion of auger Open
																		No free water

	IECT Proposed Development - Wilmot E ATION New Hamburg, Ontario NG METHOD Continuous Flight Hollow S		-					BORI	NG DA	I TE Ju	ine 6, 2	018		E	PML RE ENGINE ECHNI	ER		oghrin
	SOIL PROFILE		Ū		PLES	SCALE	SHEA + FIFI	R STR		H (kPa) RVANE	0.00	PI AST						
	DESCRIPTION SURFACE ELEVATION TOPSOIL: Dark brown silt, moist	STRAT PLOT	NUMBER	ТҮРЕ	"N" VALUES	ELEVATION SC/	DYNAI STANI	50 1 MIC CON DARD P	00 1 NE PEN ENETRA	ETRATION T	00	W _P			WL	d GAS READINGS		GROUND WATE OBSERVATION AND REMARKS DISTRIBUTH GR SA
0.40	CLAYEY SILT: Firm to stiff brown clayey silt, some sand, trace gravel, APL		1	SS	7									0				Set in Concrete
			2	SS	12							Þ	1	o				Bentonite Seal
<u>4.0</u>	becoming firm grey occasional silt layers		3	SS	9		•							0				
			4	SS	8		•							0				Filter Sand
6.7			5	SS	8								c					•
	BOREHOLE TERMINATED AT 6.7 m																Initia	<u>er Level Readings:</u> l: Dry -06-15: 2.91 m

LO	DJECT Proposed Development - Wilmot E CATION New Hamburg, Ontario RING METHOD Continuous Flight Hollow S				s Eastside			RING DA			018		EN	IL REF GINEI CHNIC	ER	18KF(W. Lo W. Lo	ghrin
DEPT	SOIL PROFILE	LOT	R		PLES	IN SCALE	SHEAR S [™] +FIELD V/ ▲POCKET 50	NE ∆TO PENETRO	H (kPa) RVANE DMETER 50 20	0 Qu 0 Q	PLAST LIMIT WP	ric Nat Mois Con	TURAL STURE NTENT W	Liquid Limit WL	READINGS	(ROUND WATER
ELE (metre	s) SURFACE ELEVATION	STRAT PLOT	NUMBER	ТҮРЕ	"N" VALUES	ELEVATION	DYNAMIC C STANDARE 20	ONE PEN PENETR	-	ON × EST ●		ATER C	ONTENT	(%) 40	d GAS RE		AND REMARKS GRAIN SIZE DISTRIBUTION GR SA SI
0.30	CLAYEY SILT: Brown mottled clayey silt, some sand trace gravel, occasional wet		1	SS	5		•						o			¥ ¥	Stickup Well Protect Set in Concrete
	sand layers, APL		2	SS	7							0					
_ <u>2.</u> 1	becoming hard, DTPL		3	SS	6							0					Bentonite Seal
			4	SS	40						0						
			5	SS	30	-											
4.0	SILTY SAND: Dense brown silty fine sand, saturated																Filter Sand
			6	SS	54							0					Slotted Screen
6.7	BOREHOLE TERMINATED AT 6.7 m		7	SS	44							0				Free v	vater at 3.5 m after S
																Initial:	<u>Level Readings:</u> 3.5 m)6-15: 2.28 m

	JECT Proposed Development - Wilmot E	Emplo	yme	nt Land	s Eastside						c				ML RE		18KF	
	ATION New Hamburg, Ontario ING METHOD Continuous Flight Hollow S	stem /	Auge	ers				BORI	NG DA	TE Jun	e 6, 20	018			NGINE ECHNI			oghrin oghrin
	SOIL PROFILE			SAN	PLES	CALE	SHEA +FIEL	R STRI		H (kPa) RVANE METER	O Qu	PLAST LIMIT						GROUND WATER
<u>EPTH</u> ELEV etres)	DESCRIPTION	STRAT PLOT	NUMBER	ТҮРЕ	"N" VALUES	ELEVATION SCALE	5 DYNAN STAND	0 10 NIC CON OARD PE	0 1 IE PENE ENETRA		D N × ST ●	W _P	ATER C		WL	g GAS READINGS		OBSERVATIONS AND REMARKS GRAIN SIZI DISTRIBUTION GR SA SI
0.35	TOPSOIL: Dark brown silt, moist CLAYEY SILT: Firm brown clayey silt, some sand, trace gravel, APL, occasional wet silt layers			SS	9	_	•						0					Stickup Well Prote
<u>2.5</u>	becoming grey		2	SS	8	_	•					×		0				Bentonite Seal
			3	SS	6	_	•							0				
			4	SS	9		•							0				Filter Sand
			5	SS	10								0					Slotted Screen
6.7	BOREHOLE TERMINATED AT 6.7 m				2												Initial	<u>r Level Readings:</u> : Dry -06-15: 6.12 m

TION New Hamburg, Ontario NG METHOD Continuous Flight Hollow S				s Eastside					e 9, 20	018		EN		ER	18KFC W. Log W. Log	ghrin
SOIL PROFILE			SAM	PLES	ALE	SHEAR ST +FIELD VA	RENGTH	H (kPa) RVANE	⊖ Qu	PLAST			LIQUID	es a		ROUND WATER
DESCRIPTION SURFACE ELEVATION	STRAT PLOT	NUMBER	ТҮРЕ	"N" VALUES	ELEVATION SC	APOCKETI 50	PENETRO	OMETER 50 200 ETRATION ATION TE	οα D N × ST •	W _P			W _L	mdd GAS READIN		DBSERVATIONS AND REMARKS GRAIN SIZE DISTRIBUTION GR SA SI Stickup Well Prote
CLAYEY SILT: Firm to very stiff brown	fīŤ	1	SS	9							0					Set in Concrete
to DTPL, occasional silt layers		2	SS	7								0				
		3	SS	11								0				Bentonite Seal
		4	SS	13		+						0				
becoming grey, occasional saturated silt layers																Filter Sand
		5	SS	6							¢					Slotted Screen
SILT TILL: Very dense grey silt, some sand, some gravel, occasional cobble, occasional boulders, moist	· · · ·	6	55	75						0						
BOREHOLE TERMINATED AT 6.7 m			33	13											Initial:	<u>Level Readings:</u> Dry)6-15: 1.56 m
	VG METHOD Continuous Flight Hollow S SOIL PROFILE DESCRIPTION SURFACE ELEVATION TOPSOIL: Dark brown silt, moist CLAYEY SILT: Firm to very stiff brown clayey silt, some sand, trace gravel, APL to DTPL, occasional silt layers DESCRIPTION becoming grey, occasional saturated silt layers SILT TILL: Very dense grey silt, some sand, some gravel, occasional cobble, occasional boulders, moist	VG METHOD Continuous Flight Hollow Stem A SOIL PROFILE DESCRIPTION SURFACE ELEVATION TOPSOIL: Dark brown silt, moist CLAYEY SILT: Firm to very stiff brown clayey silt, some sand, trace gravel, APL to DTPL, occasional silt layers Image: Clayer Silt Silt Silt Silt Silt Silt Silt Silt	NG METHOD Continuous Flight Hollow Stem Augers SOIL PROFILE Industry DESCRIPTION Industry SURFACE ELEVATION 1 TOPSOIL: Dark brown silt, moist 1 CLAYEY SILT: Firm to very stiff brown clayey silt, some sand, trace gravel, APL to DTPL, occasional silt layers 2 3 4 becoming grey, occasional saturated silt layers 5 SILT TILL: Very dense grey silt, some sand, some gravel, occasional cobble, occasional boulders, moist 6	NG METHOD Continuous Flight Hollow Stem Augers SOIL PROFILE SAM DESCRIPTION I SURFACE ELEVATION 1 TOPSOIL: Dark brown silt, moist 1 CLAYEY SILT: Firm to very stiff brown clayey silt, some sand, trace gravel, APL to DTPL, occasional silt layers 1 Start Start 3 SS 3 SS 3 SS 5 SS 5 SILT TILL: Very dense grey silt, some sand, some gravel, occasional cobble, occasional boulders, moist 0	NG METHOD Continuous Flight Hollow Stem Augers SOIL PROFILE SAMPLES DESCRIPTION I SS 9 SURFACE ELEVATION TOPSOIL: Dark brown silt, moist 1 SS 9 CLAYEY SILT: Firm to very stiff brown clayey silt, some sand, trace gravel, APL to DTPL, occasional silt layers 1 SS 7 4 SS 11 5 SS 6 SILT TILL: Very dense grey silt, some sand, some gravel, occasional cobble, occasional boulders, moist 1 SS 75	NG METHOD Continuous Flight Hollow Stem Augers SOIL PROFILE SAMPLES DESCRIPTION URFACE ELEVATION TOPSOIL: Dark brown silt, moist TOPSOIL: Dark brown silt, moist CLAYEY SILT: Firm to very stiff brown clayey silt, some sand, trace gravel, APL 0 4 SS 1 SS 9 2 SS 7 3 SS 11 4 SS 13 becoming grey, occasional saturated silt 5 SS 5 SS 6 6 SS 75	NG METHOD Continuous Flight Hollow Stem Augers SOIL PROFILE SAMPLES U SILE SAMPLES U DESCRIPTION U U SILE RATION TOPSOIL: Dark brown silt, moist SILT Firm to very stiff brown clayey silt, some sand, trace gravel, APL to DTPL, occasional silt layers SS 7 4 SS 13 5 SS 6 SILT TILL: Very dense grey silt, some sand, some gravel, occasional cobble, occasional boulders, moist 1	NG METHOD Continuous Flight Hollow Stem Augers SOIL PROFILE SAMPLES UPON SAMPLES DESCRIPTION SURFACE ELEVATION SURFACE ELEVATION 1 SS 9 SURFACE ELEVATION 1 SS 9 CLAVEY SILT: Firm to very stiff brown clayey silt, some sand, trace gravel, APL to DTPL, occasional silt layers 1 SS 7 3 SS 11 SS 9	NG METHOD Continuous Flight Hollow Stem Augers SOIL PROFILE SAMPLES If ELD VANE ATORVANE DESCRIPTION If I I I I I I I I I I I I I I I I I I	NO METHOD Continuous Flight Hollow Stem Augers SOIL PROFILE SAMPLES DESCRIPTION Description <thdescription< th=""> Description</thdescription<>	NO METHOD Continuous Flight Hollow Stem Augers SOIL PROFILE SAMPLES BLAR STRENGTH (kPa) +FIELD VANE △TORVANE ○ Ou PLASS DESCRIPTION U U U SHEAR STRENGTH (kPa) +FIELD VANE △TORVANE ○ Ou PLASS POCKET PENETRATION TEST ○ U PLASS SURFACE ELEVATION U	NOMETHOD Continuous Flight Hollow Stem Augers SOIL PROFILE SAMPLES DESCRIPTION IO IO <thio< th=""> IO IO IO<</thio<>	SOIL PROFILE SAMPLES Image: Solid profile Samples Samples	SOIL PROFILE SAMPLES Image: Continuous Flight Hollow Stem Augers Image: Context Presentation Stem	MEMETHOD Continuous Flight Hollow Stem Augers TECHNICAL SOIL PROFILE SAMPLES Image: Contract of the status of the s	MS METHOD Continuous Flight Hollow Stem Augers TECHNICAN W. Log SOLL PROFILE SAMPLES Image: Sample S

	CATION New Hamburg, Ontario RING METHOD Continuous Flight Hollow S SOIL PROFILE	tem	Auge		IPLES		SHEAR	STREN	DATE Ju)	-		1			W. Loghrin W. Loghrin
EPTI LEV etre	description	STRAT PLOT	NUMBER		N" - VALUES	ELEVATION SCALE	+FIELD ▲POCKI 50 UYNAMIC STANDAI	VANE A ET PENE 100 CONE F RD PENE	TORVANE TROMETER 150 2 ENETRATI TRATION T	OQU QO QO ON × EST •	W _P	ATER (w 	GAS READ	GROUND WATEI OBSERVATIONS AND REMARKS GRAIN SI DISTRIBUTIC GR SA S
	SURFACE ELEVATION TOPSOIL: Dark brown clayey silt, APL CLAYEY SILT: Very stiff brown clayey	Ť	1	SS	5		20	40	60 8	80		0 20 0	0 30	40	ppm	GR SA S
	silt, some sand, trace gravel, DTPL		2	SS	27	_		>				0				
			3	SS	18							ο				
			4	SS	14	_					ŀ		0			
			5	SS	12		•						0			
<u>4.0</u>	becoming grey, APL, occasional wet silt layers															
			6	SS	12		•					1	0			
			7	ss	16							0				
<u>6.7</u>	BOREHOLE TERMINATED AT 6.7 m											0		_		Upon completion of augo
																No free water

LOCA	ECT Proposed Development - Wilmot I ITION New Hamburg, Ontario NG METHOD Continuous Flight Hollow S		-		s Eastside			BORI	NG DA	I TE Jur	ne 9, 20	018			PML ENG TEC	INEE	R	18KF025 W. Loghrin W. Loghrin
	SOIL PROFILE			SAM	PLES	ЧГШ	SHEA	R STR		H (kPa) RVANE	0.00	PI AS		ATURA	L 11	סוווס	SS	
<u>EPTH</u> ELEV netres)	DESCRIPTION	STRAT PLOT	NUMBER	ТҮРЕ	"N" VALUES	ELEVATION SCALE	DYNA STANI	50 1 MIC COM DARD PI	00 1 NE PEN ENETRA	RVANE DMETER 50 20 ETRATIC ATION TE	N ×	W _P	ATER		ENT (%		GAS READ	GROUND WATEF OBSERVATIONS AND REMARKS GRAIN SIZ DISTRIBUTIO GR SA S
	SURFACE ELEVATION TOPSOIL: Dark brown silt, moist CLAYEY SILT: Firm brown clayey silt,	Ĩ	1	SS	4		•	20 4	06	50 80	J		02	0 30 0) 40	,	ppm	GR SA S
	some sand, trace gravel, APL to DTPL		2	SS	9	-								0				
<u>1.4</u>	becoming hard, DTPL		3	SS	34	_							0					
					40	-							0					
<u>2.9</u>	becoming grey	++++	4	SS	40	-							0					
			5	SS	31	_							0					
			6	SS	34								0					
6.7	BOREHOLE TERMINATED AT 6.7 m		7	SS	30			-				0	>					
																		Upon completion of auge Open No free water

ID Number: TT1-18

Project: Hydrogeological Investigation

Project No: 34896-104 & 39219-104

Client: Badenview Developments Inc. & New HamburgIrs Inc.

Site Location: New Hamburg, ON

Date: 7/20/2018

Contractor: T. Musselman Excavating

Excavation Method: Track-Mounted Excavator

	SUBSURFACE PROFILE			HEADSPACE
Symbol	Soil Description	Elevation (masl) Depth (m)	Soil Sample Lab Analysis	VOC ppm 20 40 60 8 Hydrocarbon ▼ ppm 100 200 300 40
m	Ground Surface	0.0		
	TOPSOIL Dark brown topsoil, rootlets, damp	0.0		
- ~		-0.6 0.6		
-	SANDY SILT Brown sandy silt, some stones, damp to slightly moist	-1.2		
- - - - - 2	SILTY SAND Brown silty sand, trace clay, moist to very moist. Mottling observed at approximately 1.8 m.	1.2		
-		-2.0		
- 2 - -	increasing silt and moisture content	2.0		
-		-2.7		
-	SANDY SILT Grey sandy silt, trace clay, very moist to wet	2.7 -3.0		
	increasing sand content, wet	-4.4		
	Excavation Terminated	4.4		

Drafted by: KLW

Reviewed by: PAG



Pooling observed (upwelling) upon completion. Test trench collapse occurred within silty sand layer. Approximately 10-15cm at base after ~4.5 hours elapsed.

ID Number: TT2-18

Project: Hydrogeological Investigation

Project No: 34896-104 & 39219-104

Client: Badenview Developments Inc. & New HamburgIrs Inc.

Site Location: New Hamburg, ON

Date: 7/20/2018

Contractor: T. Musselman Excavating

Excavation Method: Track-Mounted Excavator

		SUBSURFACE PROFILE			HEADSPACE	
Depth	Symbol	Soil Description	Elevation (masl) Depth (m)	Soil Sample Lab Analysis	VOC ppm 20 40 60 80 Hydrocarbon ppm 100 200 300 400	
ft_m		Ground Surface	0.0			
0 ft m 0 - 0	$l_{j}l_{j}l_{j}l_{j}l_{j}l_{j}$	TOPSOIL Dark brown topsoil, rootiets, damp	-0.6			
2		SAND	0.6			
		Brown fine-grained sand, some silt, damp	-0.9 0.9			
4 6 10 12 12 14 14 14 14 14 14 16 18 10 10 12 10 10 10 10 10 10 10 10 10 10		Excavation Terminated				
			Notes: Test	rench abandoned bec	ause tile drainage nine	
Draf	Field Technician: FAH Drafted by: KLW Reviewed by: PAG Sheet: 1 of 1					

ID Number: TT3-18

Project: Hydrogeological Investigation

Project No: 34896-104 & 39219-104

Client: Badenview Developments Inc. & New HamburgIrs Inc.

Site Location: New Hamburg, ON

Date: 7/20/2018

Contractor: T. Musselman Excavating

Excavation Method: Track-Mounted Excavator

		SUBSURFACE PROFILE			HEADSPACE
Depth	Symbol	Soil Description	Elevation (masl) Depth (m)	Soil Sample Lab Analysis	VOC ppm 20 40 60 80 Hydrocarbon ppm 100 200 300 400
$0\frac{\text{ft}}{\exists}0$		Ground Surface	0.0		
	$l_j l_j l_j l_j$	TOPSOIL Dark brown topsoil, rootlets, damp	0.0 -0.5		
2		CLAYEY SILT TILL Brown clayey silt till, some stones, some sand, damp	0.5		
4 4 6 1 1 1 1 1 1 1 1 1 1 1 1 1		reduced sand content	-1.2		
1	4	transitioning to grey	-2.9 2.9		
10 	########	SILTY CLAY TILL Grey silty clay till, damp			
-	Ħ		-4.6		
	1	SANDY SILT CLAY TILL Grey sandy silt clay till, damp to moist, seams of very high moisture	4.6		
16 17 18 20 20 22 22 22		Grey sandy sit clay till, damp to moist, seams of very nigh moisture Excavation Terminated	<u>-4.9</u> 4.9		
F		M			1m x 1 4m \\/ x 4 0m D
Field	d Te	chnician: FAH		avation Dimensions: 2. eepage or pooling upor	1m L x 1.4m W x 4.9m D

Drafted by: KLW

Reviewed by: PAG



No visible seepage or pooling upon completion. Slight pooling (unmeasureable) at base after ~4.75 hours elapsed.

ID Number: TT4-18

Project: Hydrogeological Investigation

Project No: 34896-104 & 39219-104

Client: Badenview Developments Inc. & New HamburgIrs Inc.

Site Location: New Hamburg, ON

Date: 7/20/2018

Contractor: T. Musselman Excavating

Excavation Method: Track-Mounted Excavator

		SUBSURFACE PROFILE			HEADSPACE
Depth	Symbol	Soil Description	Elevation (masl) Depth (m)	Soil Sample Lab Analysis	VOC ppm ■ 20 40 60 80 Hydrocarbon ▼ ppm ▼ 100 200 300 400
ft m		Ground Surface	0.0		
	$l_{j}l_{j}l_{j}l_{j}$	TOPSOIL Dark brown topsoil, rootlets, damp	0.0 -0.5		
2		SAND Light brown fine grained sand, trace silt, damp to slightly moist	0.5		
			-1.2 1.2		
6 		SILT TILL Brown silt till, some clay, trace sand, trace stones, damp to moist			
8		becoming moist to very moist and transitioning to grey	-2.1 2.1		
10		becoming very moist to saturated	-3.0 3.0		
		grey, some sand, very moist to wet	-3.7 3.7		
	ŁĨ.		-4.1 4.1		
14		Excavation Terminated	7.1		
18					
18 18 20 1 18 1 10 1 10 10 10 10 10 10 10 10 10 10 10					
22-					

Field Technician: FAH

Drafted by: KLW

Reviewed by: PAG



Notes: Excavation Dimensions: 4.0m W x 2.7m L x 4.1m D

Minor pooling (upwelling) of water from center of excavation upon completion. Approximately 5-10cm of water at base after \sim 6.25 hours elapsed.

ID Number: TT5-18

Project: Hydrogeological Investigation

Project No: 34896-104 & 39219-104

Client: Badenview Developments Inc. & New HamburgIrs Inc.

Site Location: New Hamburg, ON

Date: 7/20/2018

Contractor: T. Musselman Excavating

Excavation Method: Track-Mounted Excavator

			SUBSURFACE PROFILE			HEADSPACE
4400	nepul	Symbol	Soil Description	Elevation (masl) Depth (m)	Soil Sample Lab Analysis	VOC ppm 20 40 60 80 Hydrocarbon ppm 100 200 300 400
ft	m		Ground Surface	0.0		
0 	-	$l_{j}l_{j}l_{j}l_{j}$	TOPSOIL Dark brown topsoil, rootlets, damp	0.0 -0.5		
2	-		SAND Light brown fine grained sand, trace silt, damp to slightly moist	0.5		
4	_			-1.2 1.2		
	-		CLAYEY SILT TILL Brown clayey silt till, damp			
6	-	Ŀ		- <u>-1.8</u> 1.8		
6 8 8	- 2 - -	#1#1#1	SILTY CLAY TILL Grey silty clay till, damp to slightly moist	1.0		
10		1/#/#//	transitioning from moist to very moist	- <u>-3.0</u> 3.0		
12	- - - 4	HHHH	wet below 4.0 m	-4.0 4.0 -4.3		
14			Excavation Terminated	4.3		
16			Excavation reminated			
18	_					
18	_ _ 6					
22						

Field Technician: FAH

Drafted by: KLW

Reviewed by: PAG



Notes: Excavation Dimensions: 2.4m L x 1.4m W x 4.3m D

No visible seepage or pooling upon completion. Less than 5cm at base after ${\sim}5.5$ hours elapsed.

ID Number: TT6-18

Project: Hydrogeological Investigation

Project No: 34896-104 & 39219-104

Client: Badenview Developments Inc. & New HamburgIrs Inc.

Site Location: New Hamburg, ON

Date: 10/25/2018

Contractor: T. Musselman Excavating

Excavation Method: Track-Mounted Excavator

	SUBSURFACE PROFILE				HEADSPACE
Depth	Symbol	Soil Description	Elevation (masl) Depth (m)	Soil Sample Lab Analysis	VOC ppm 20 40 60 80 Hydrocarbon ppm 100 200 300 400
$0\frac{\text{ft}}{3}$ m	~	Ground Surface	0.0		
0 1 2 1 4 1 4 1 1 1 1 1 1 1 1 1 1 1 1 1		COULD CUILD CUILD Dark brown slit topsoil, some clay, moist CLAYEY SILT TILL Brown clayey slit till, trace stones, moist SILTY CLAY TILL Grey slity clay till, trace stones, moist to wet	-0.6 0.0 -0.6 0.6 -3.0 3.0		
	Ħ		-4.9		
16 18 18 18 10 18 10 10 10 10 10 10 10 10 10 10 10 10 10		Excavation Terminated	4.9		
			Notes: Excav	ation dimensions - 1.8	m W x 5.2 m L x 4.9m D
Field Technician: KLW Notes: Excavation dimensions - 1.8m W x 5.2 m L x 4.9m D Drafted by: KLW No water observed upon completion. Approximately 2.5cm of water at base after ~30 mins elapsed. Approximately 5cm of water at base after ~5 hours elapsed. Reviewed by: PAG Sheet: 1 of 1					

ID Number: TT7-18

Project: Hydrogeological Investigation

Project No: 34896-104 & 39219-104

Client: Badenview Developments Inc. & New HamburgIrs Inc.

Site Location: New Hamburg, ON

Date: 10/25/2018

Contractor: T. Musselman Excavating

Excavation Method: Track-Mounted Excavator

		SUBSURFACE PROFILE			HEADSPACE
Depth	Symbol	Soil Description	Elevation (masl) Depth (m)	Soil Sample Lab Analysis	VOC ppm 20 40 60 80 Hydrocarbon ppm 100 200 300 400
$0\frac{\text{ft}}{1}$ m	~	Ground Surface	0.0		
2	2رارا رارا رارا را	TOPSOIL Dark brown silt topsoil, some clay, moist	-0.9 0.9		
2 2 8 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		CLAYEY SILT TILL Brown clayey silt till, trace stones, moist			
10 11 12 12 14 14 14 14 14 14 14 14 14 14 14 14 14	**	SILTY CLAY TILL Grey silty clay till, trace stones, moist to wet	-3.0 3.0		
	Ŧ	Everyation Terminated	-6.4 6.4		
22		Excavation Terminated			
Draf	Field Technician: KLW Drafted by: KLW Beviewed by: DAC				
Reviewed by: PAG Sheet: 1 of 1					

ID Number: TT8-18

Project: Hydrogeological Investigation

Project No: 34896-104 & 39219-104

Client: Badenview Developments Inc. & New HamburgIrs Inc.

Site Location: New Hamburg, ON

Date: 10/25/2018

Contractor: T. Musselman Excavating

Excavation Method: Track-Mounted Excavator

	SUBSURFACE PROFILE					HEADSPACE
Depth		Symbol	Soil Description	Elevation (masl) Depth (m)	Soil Sample Lab Analysis	VOC ppm 20 40 60 80 Hydrocarbon ppm 100 200 300 400
$0\frac{ft}{=}$	m - 0	~:	Ground Surface	0.0		
2	-	, <i>(\(\)</i> , <i>\(\)</i> , <i>\(</i>	TOPSOIL Dark brown silt topsoil, trace to some clay, moist SILT Brown silt, some clay, stoney, some cobbles, trace boulders, moist	0.0 -0.9 0.9		
6 8 10	- - - 2 - - -			-3.0 3.0		
12	- 4		SANDY SILT Brown sandy silt, wet to saturated			
18	-		Excavation Terminated	-5.5 5.5		
20	- 6 - -					
-	liala	4 7~	chnician: KI W		ation dimensions - 1.8	m W x 5.2m L x 6.4m D
	Field Technician: KLW Drafted by: KLW Reviewed by: PAG Sheet: 1 of 1					test trench observed at 20cm of water at base after

ID Number: TT9-18

Project: Hydrogeological Investigation

Project No: 34896-104 & 39219-104

Client: Badenview Developments Inc. & New HamburgIrs Inc.

Site Location: New Hamburg, ON

Date: 10/25/2018

Contractor: T. Musselman Excavating

Excavation Method: Track-Mounted Excavator

		SUBSURFACE PROFILE			HEADSPACE	
Depth	Symbol	Soil Description	Elevation (masl) Depth (m)	Soil Sample Lab Analysis	VOC ppm 20 40 60 80 Hydrocarbon ppm 100 200 300 400	
$0\frac{\text{ft}}{1}$ 0	~ .	Ground Surface	0.0			
2		TOPSOIL Dark brown silt topsoil, some clay, moist	0.0			
4 4 10 10		CLAYEY SILT TILL Brown clayey silt till, some stones, moist to wet	0.9			
12		some sand to sandy between 3.4m to 4.3m	-3.4 3.4			
		SILTY CLAY TILL Grey silty clay till, some stones, moist	-4.3 4.3			
16	7/7/7	Excavation Terminated	-5.5 5.5			
20 20 221 221						
Drat	Field Technician: KLW Drafted by: KLW Reviewed by: PAG Sheet: 1 of 1 Note: Excavation dimensions - 1.8m W x 4.6m L x 5.5m D No water at base after ~2.5 hours elapsed. Approximately 2.5cm of water at base after ~4 hours elapsed.					

ID Number: TT10-18

Project: Hydrogeological Investigation

Project No: 34896-104 & 39219-104

Client: Badenview Developments Inc. & New HamburgIrs Inc.

Site Location: New Hamburg, ON

Date: 10/25/2018

Contractor: T. Musselman Excavating

Excavation Method: Track-Mounted Excavator

		SUBSURFACE PROFILE			HEADSPACE	
Depth	Symbol	Soil Description	Elevation (masl) Depth (m)	Soil Sample Lab Analysis	VOC ppm 20 40 60 80 Hydrocarbon ppm 100 200 300 400	
$ \begin{array}{c} $	~	Ground Surface	0.0			
2	$\{\gamma_{\ell},\gamma_{\ell},\gamma_{\ell},\gamma_{\ell},\gamma_{\ell}\}$	TOPSOIL Dark brown silt topsoil, some clay, moist	0.0 -0.9 0.9			
		CLAYEY SILT TILL Brown clayey silt till, some stones, moist				
6 		SILTY CLAY TILL Trey silty clay till, some stones, some cobbles, moist	- <u>1.8</u> 1.8 - <u>5.5</u>			
20 22 22		Excavation Terminated	5.5			
Draf	Field Technician: KLW Drafted by: KLW Reviewed by: PAG Notes: Excavation dimensions - 1.8m W x 4.6m L x 5.5m D No water observed in test trench upon completion. Approximately 2.5cm of water at base after ~2 hours elapsed. Approximately 5cm of water at base after ~3.5 hours elapsed. Sheet: 1 of 1					



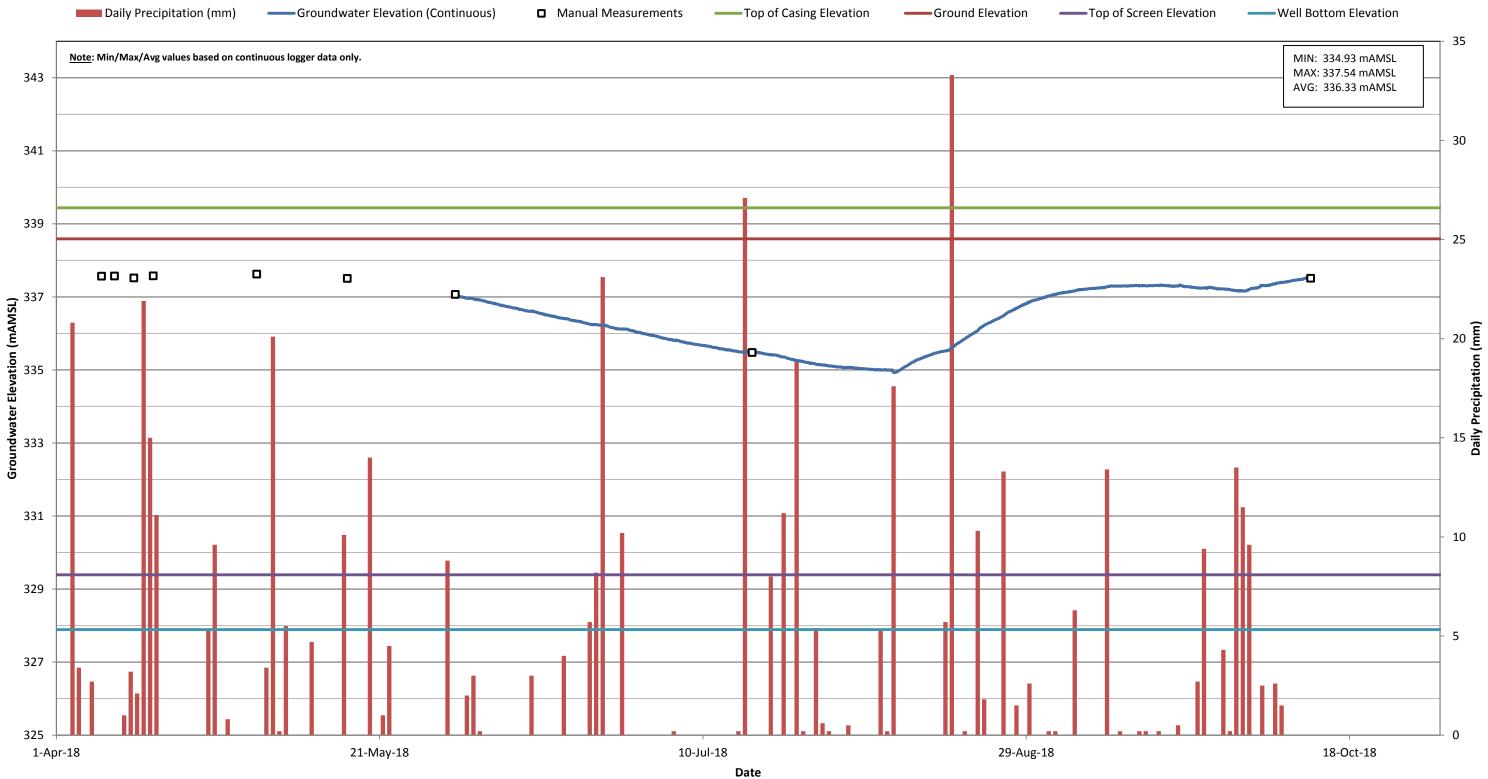
APPENDIX C

HYDROGRAPHS

Drawing on experience...Building on

gth.

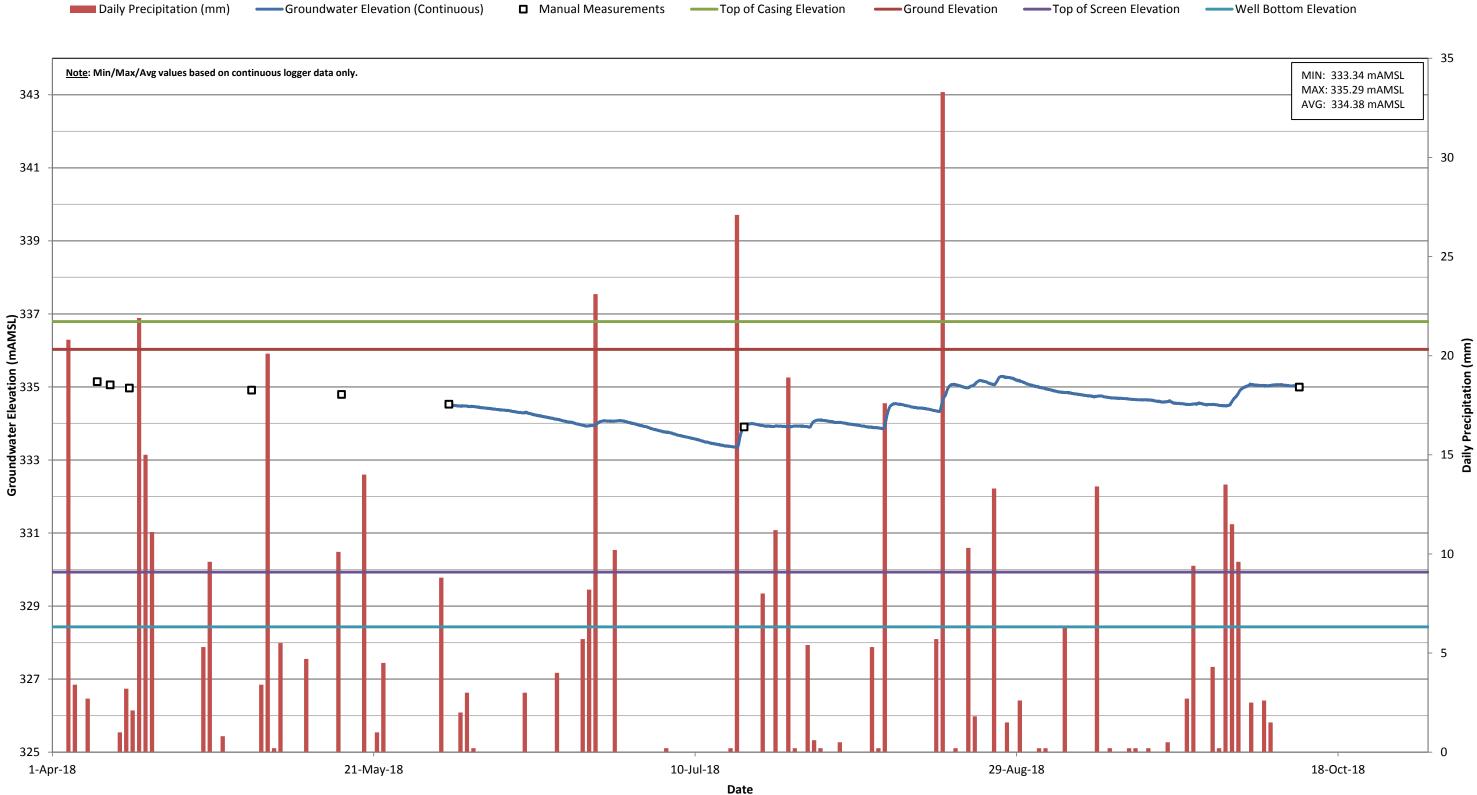
Hydrograph 1: Groundwater Elevations (mAMSL) - BH101-18





MTE File No.: 34896-104 / 39219-104 Printed on: 11/7/2018

Hydrograph 2: Groundwater Elevations (mAMSL) - BH102-18

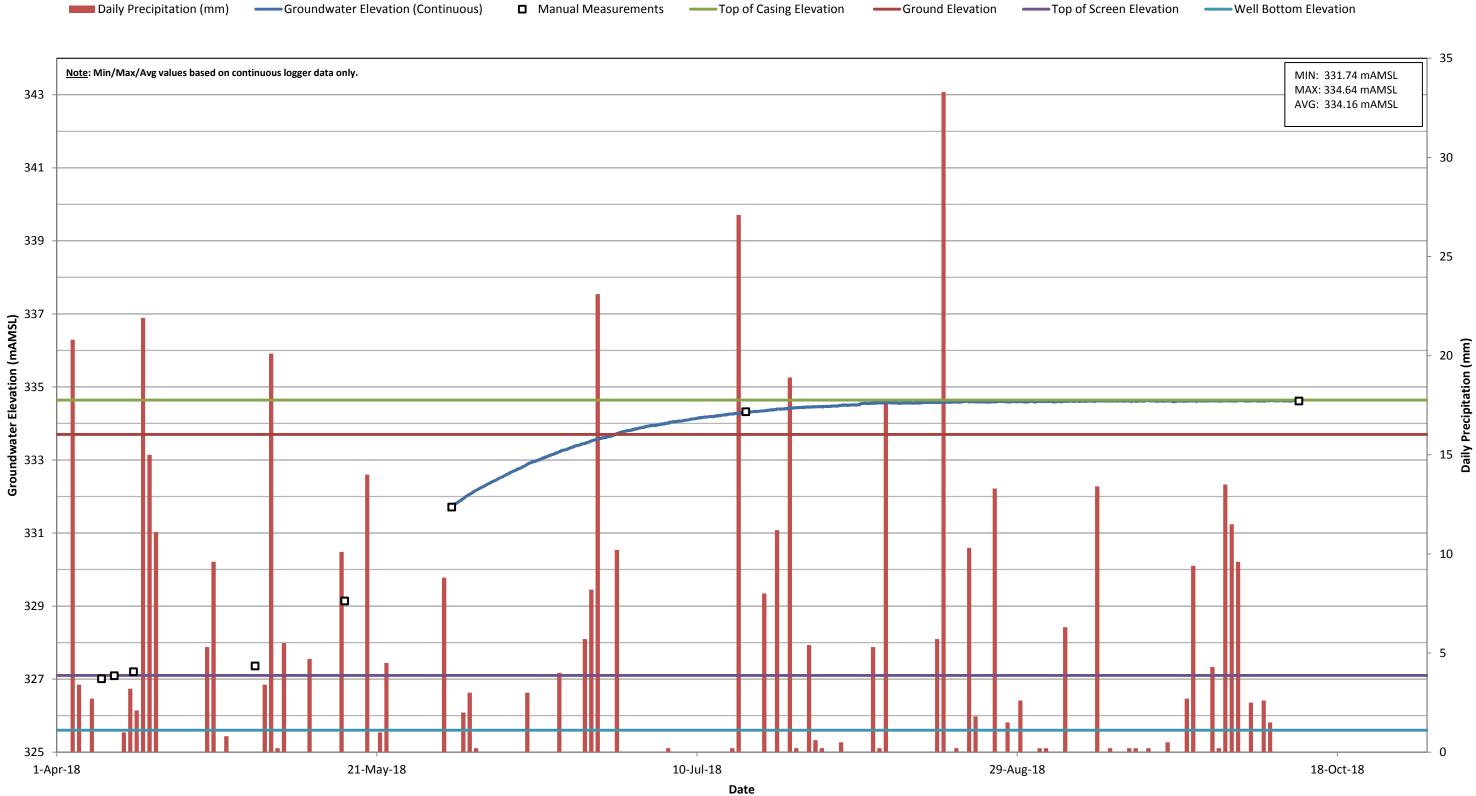




——Well Bottom Elevation

MTE File No.: 34896-104 / 39219-104 Printed on: 11/7/2018

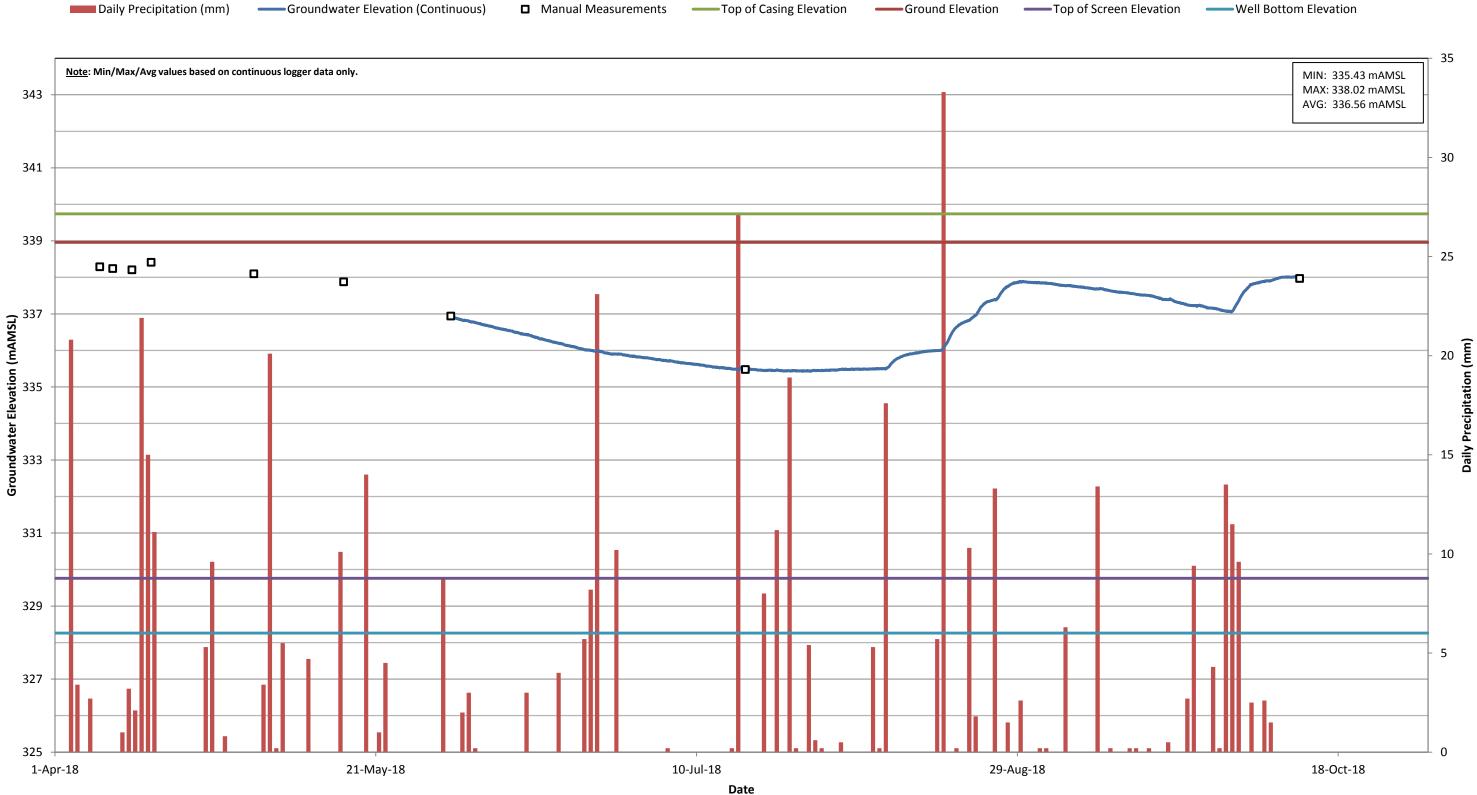
Hydrograph 3: Groundwater Elevations (mAMSL) - BH103-18





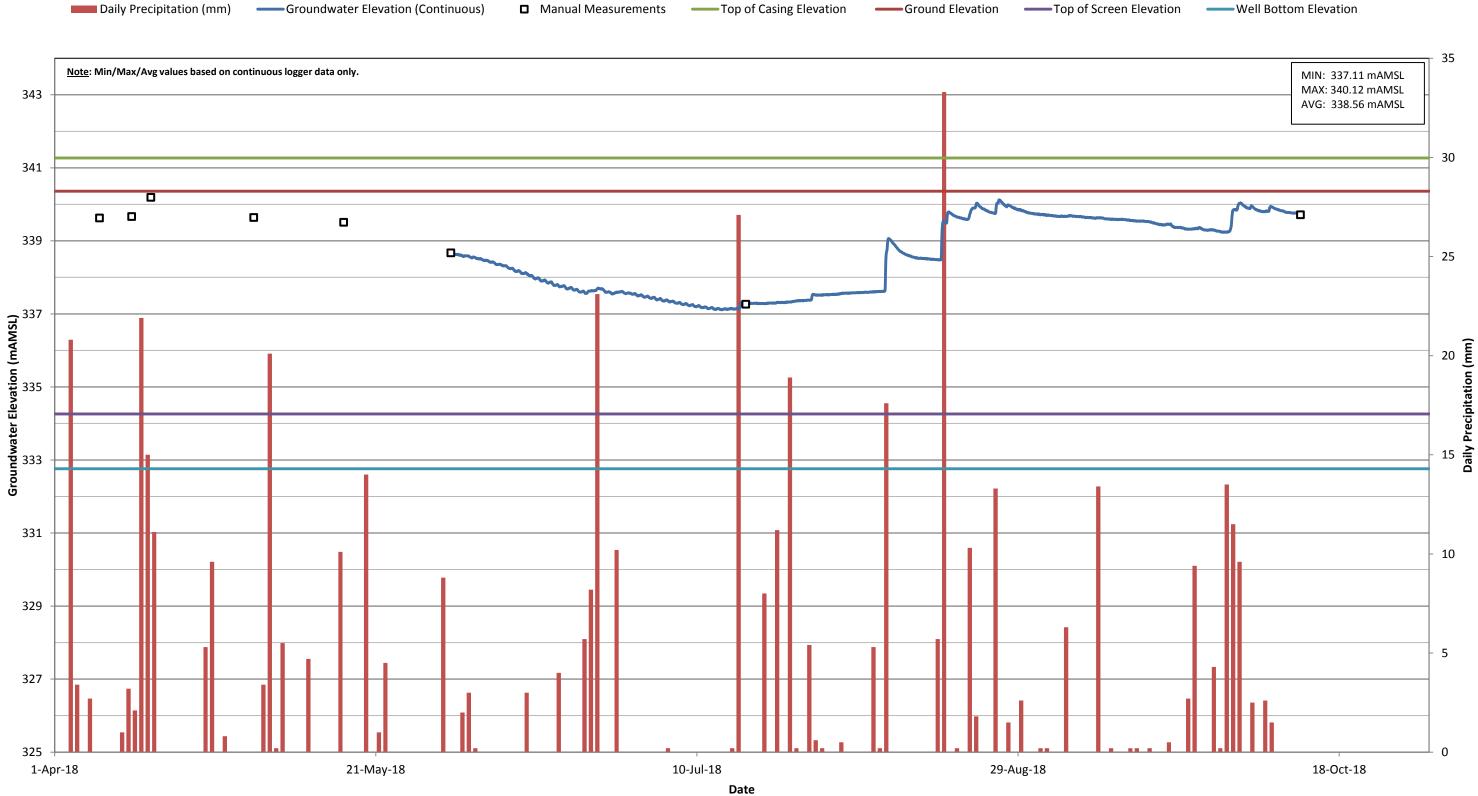
——Well Bottom Elevation

Hydrograph 4: Groundwater Elevations (mAMSL) - BH104-18





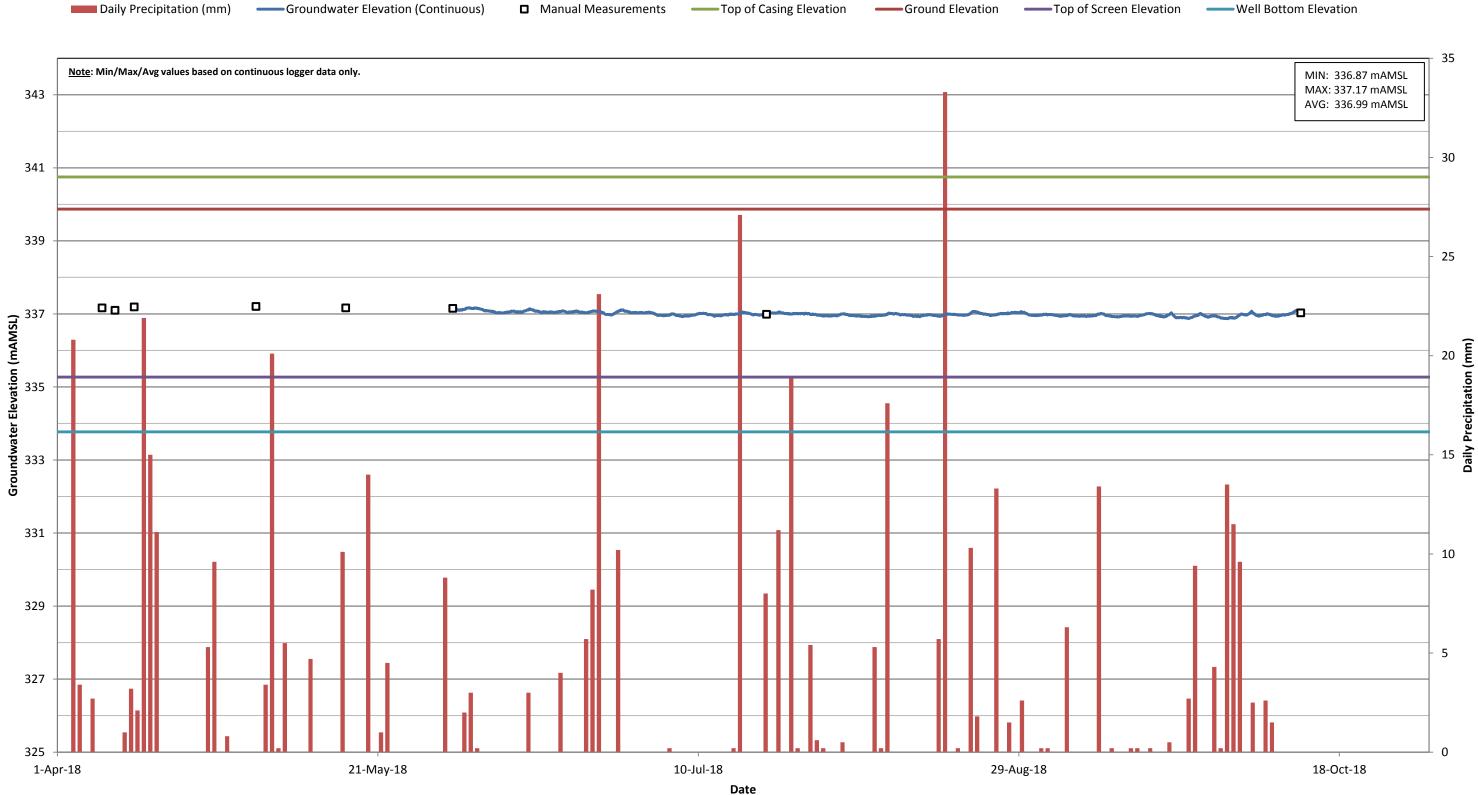
Hydrograph 5: Groundwater Elevations (mAMSL) - BH105-18





——Well Bottom Elevation

Hydrograph 6: Groundwater Elevations (mAMSL) - BH106-18





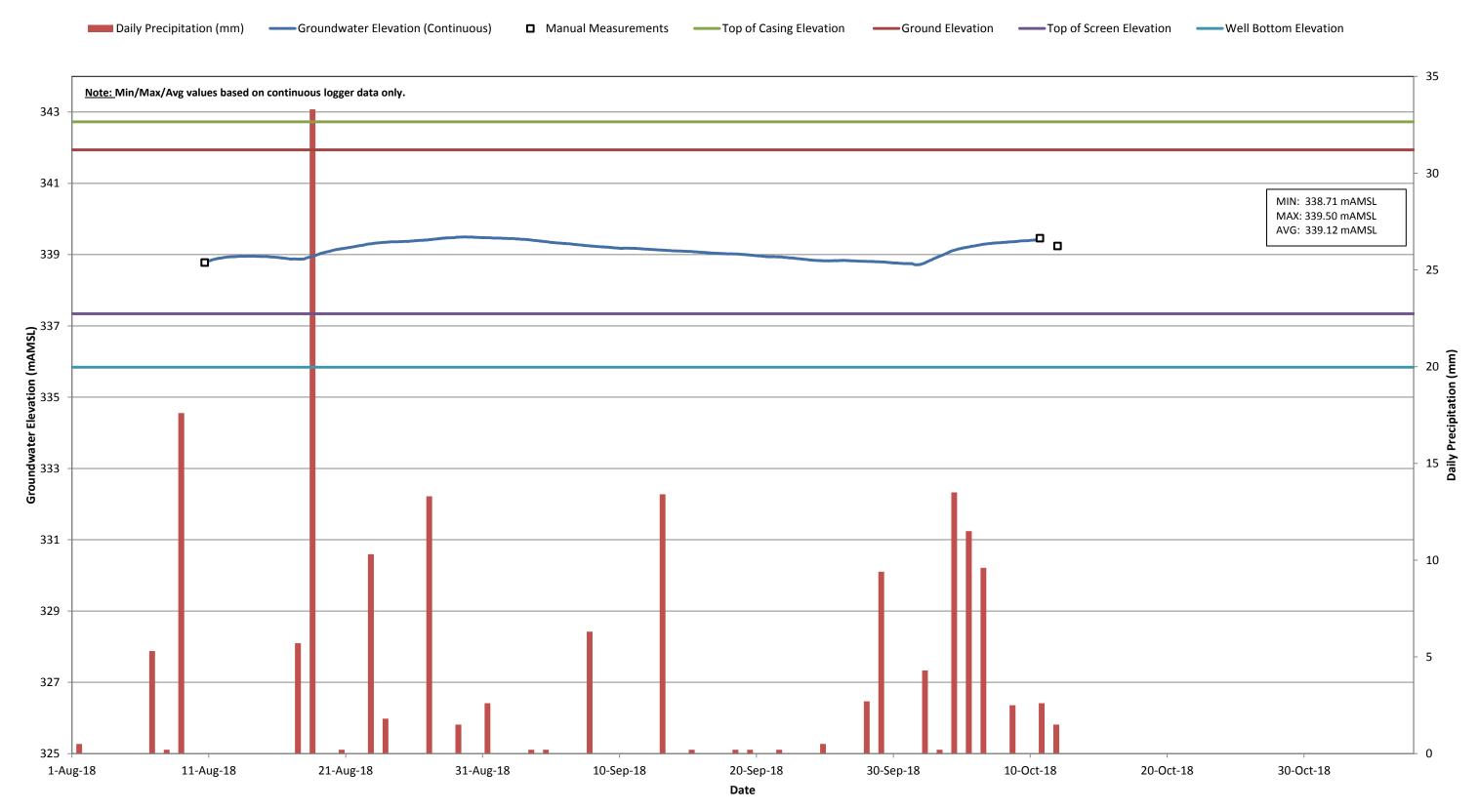


Hydrograph 7: Groundwater Elevations (mAMSL) - BH107-18



——Well Bottom Elevation

Hydrograph 8: Groundwater Elevations (mAMSL) - BH201-18





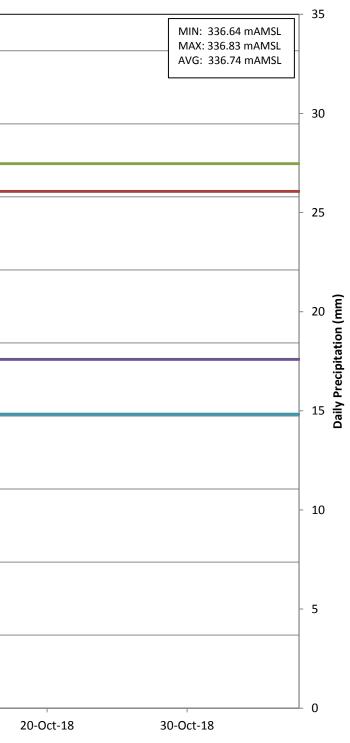
Hydrograph 9: Groundwater Elevations (mAMSL) - BH202-18

Daily Precipitation (mm) ——Groundwater Elevation (Continuous) Manual Measurements — Top of Casing Elevation Ground Elevation ——Top of Screen Elevation Note: Min/Max/Avg values based on continuous logger data only. 343 341 339 Groundwater Elevation (mAMSL) 332 332 332 332 -0 0 0 331 329 327 325 1-Aug-18 11-Aug-18 21-Aug-18 31-Aug-18 10-Sep-18 20-Sep-18 30-Sep-18 10-Oct-18 Date

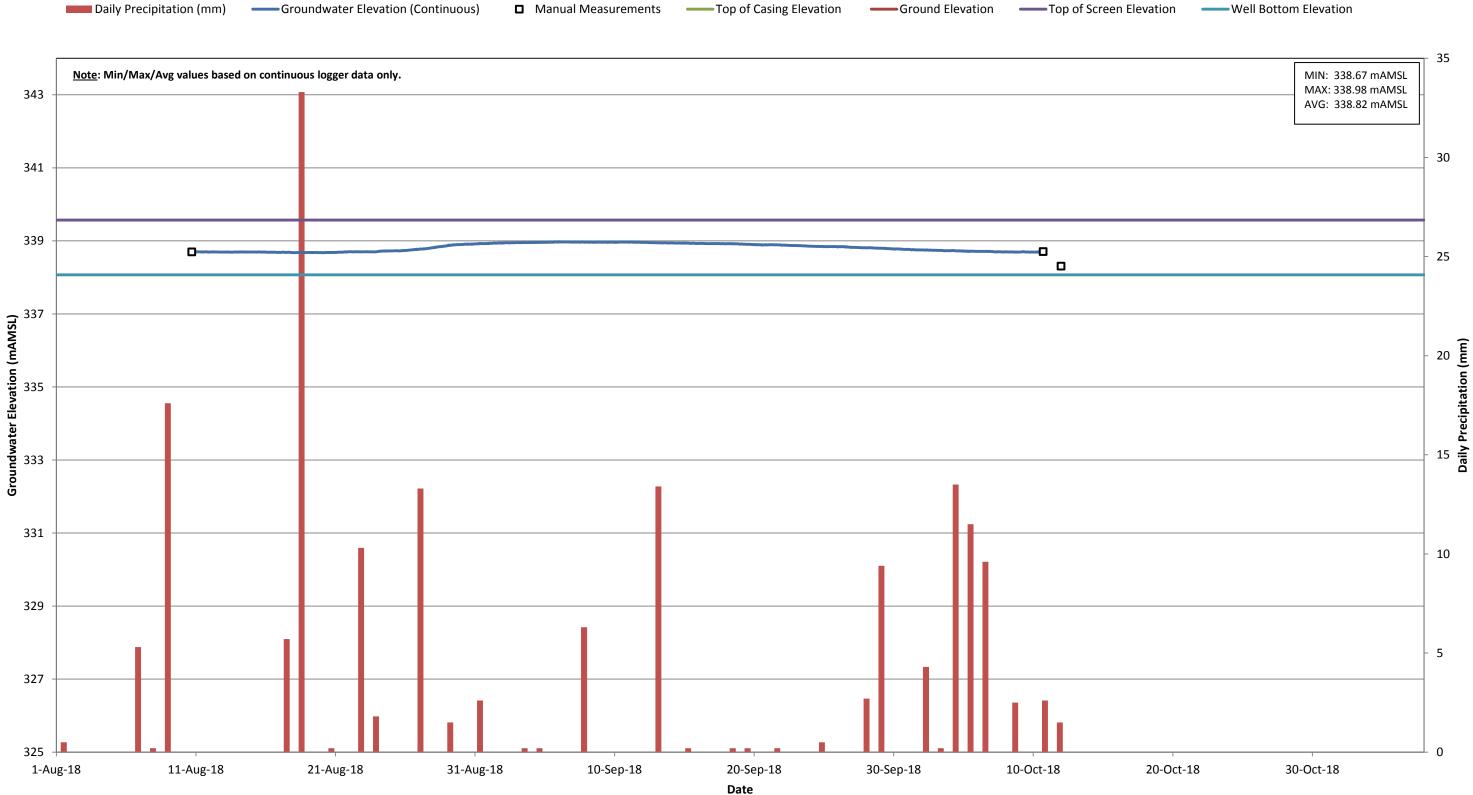
Wilmot Employment Lands / Highway 7/8 Lands Hydrogeological Investigation



levation — Well Bottom Elevation



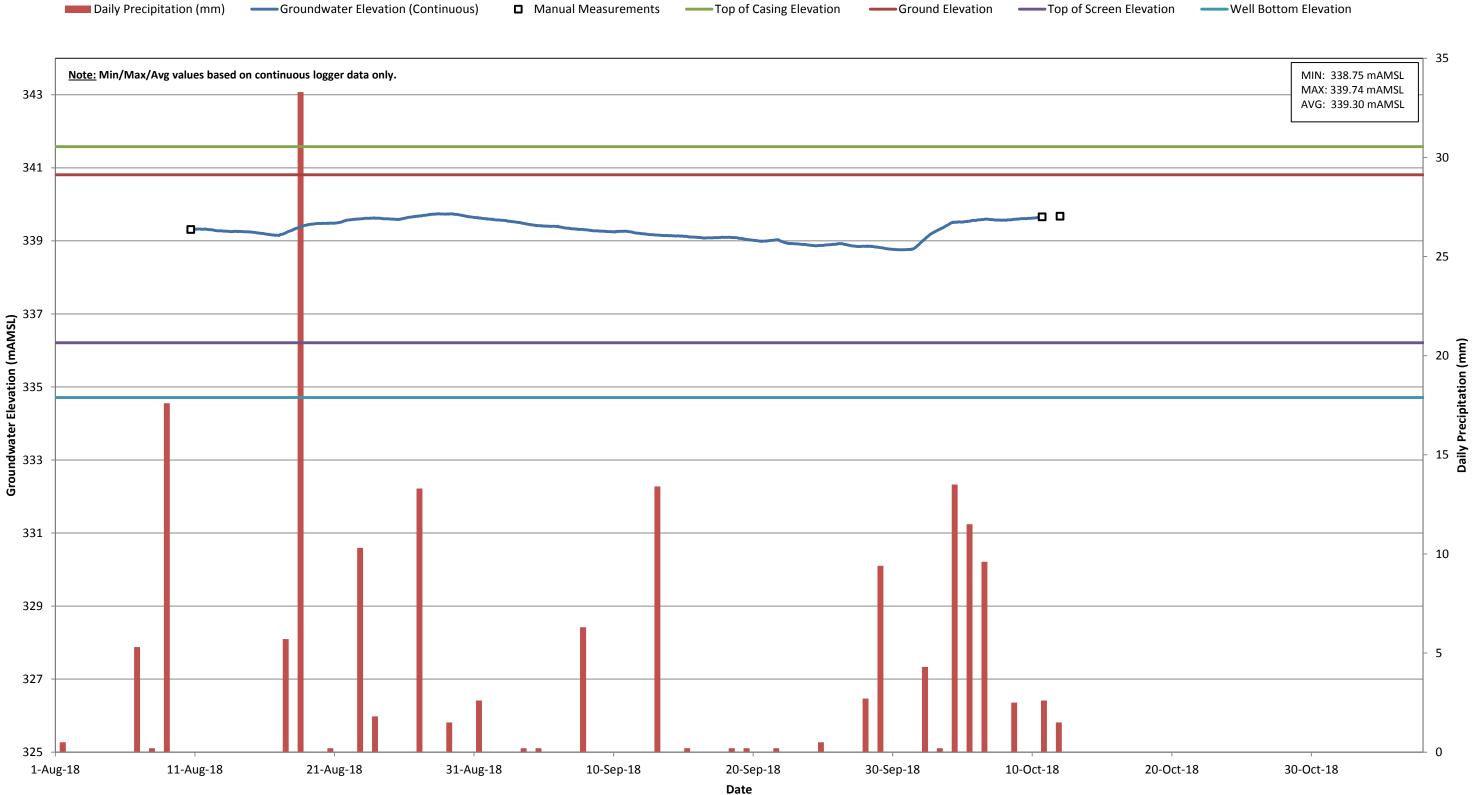
Hydrograph 10: Groundwater Elevations (mAMSL) - BH203-18



Wilmot Employment Lands / Highway 7/8 Lands Hydrogeological Investigation

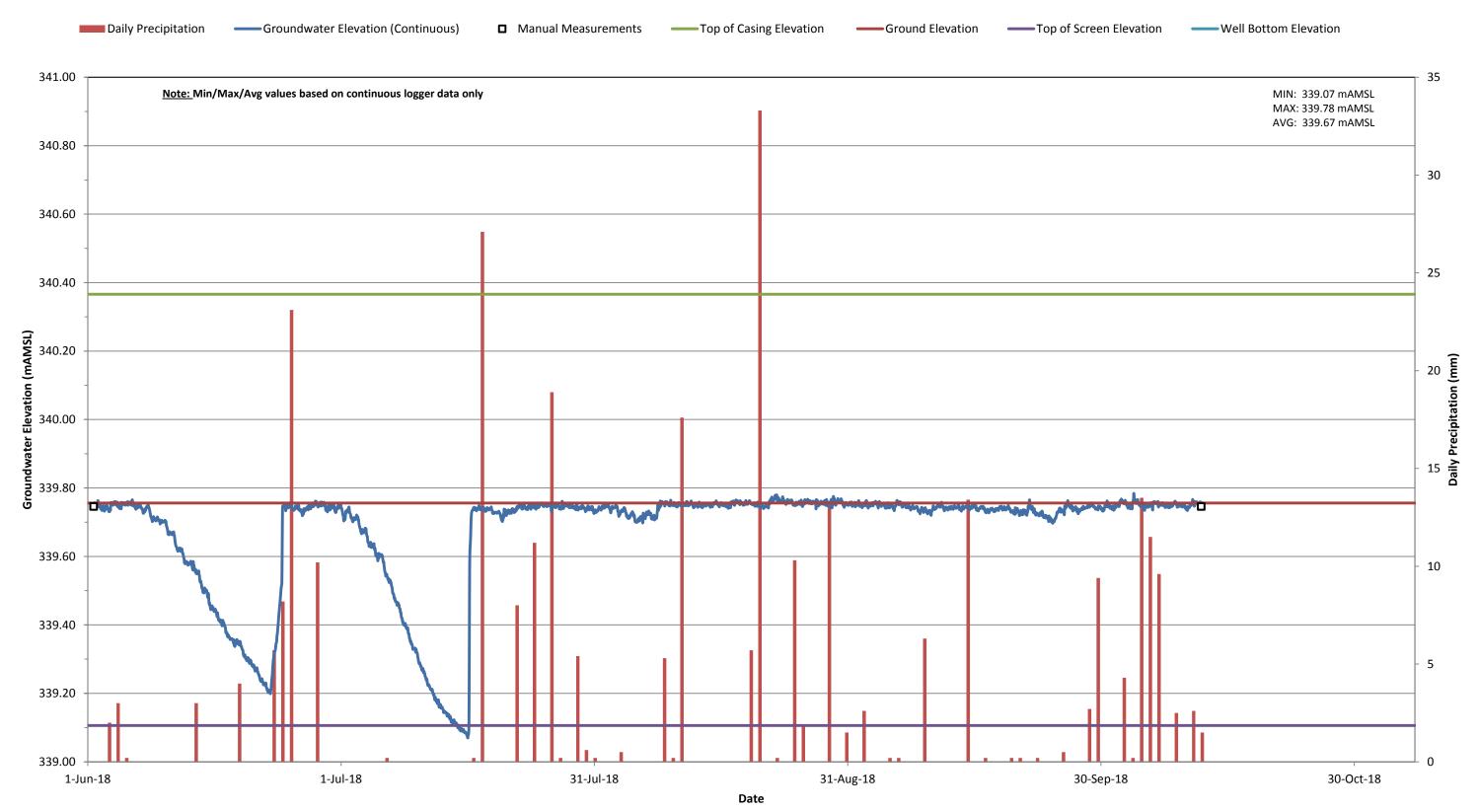


Hydrograph 11: Groundwater Elevations (mAMSL) - BH204-18



Wilmot Employment Lands / Highway 7/8 Lands Hydrogeological Investigation





Hydrograph 12: Groundwater Elevations (mAMSL) - MP3-11

Wilmot Employment Lands / Highway 7/8 Lands Hydrogeological Investigtation





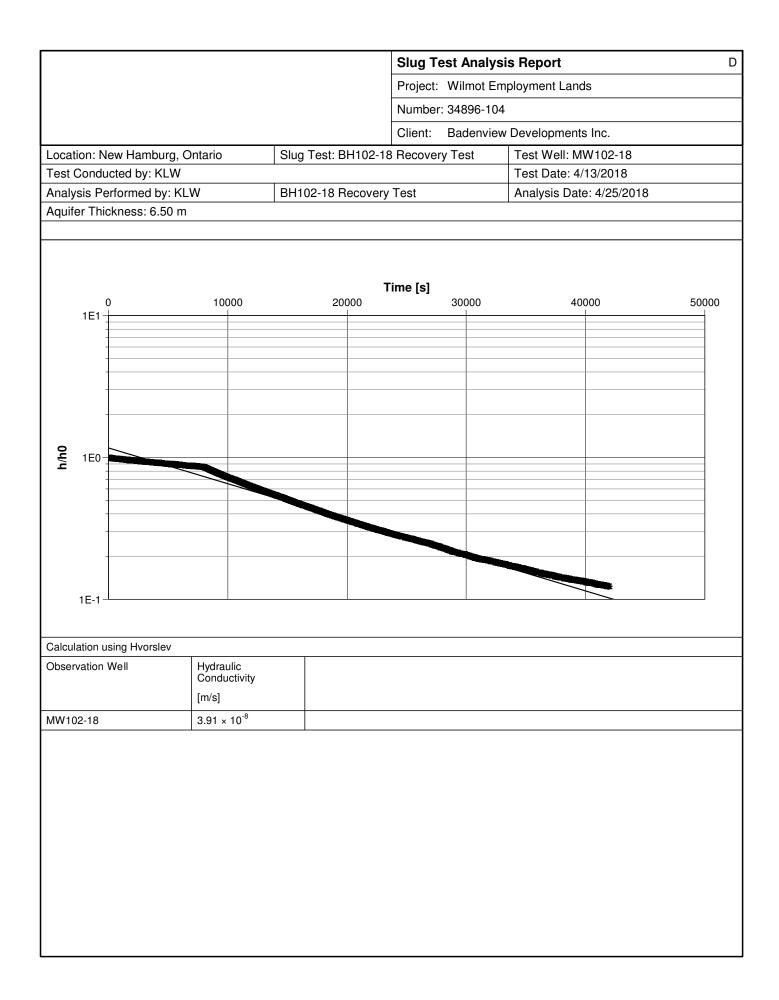
APPENDIX D

AQUIFER TEST © DATA SHEETS

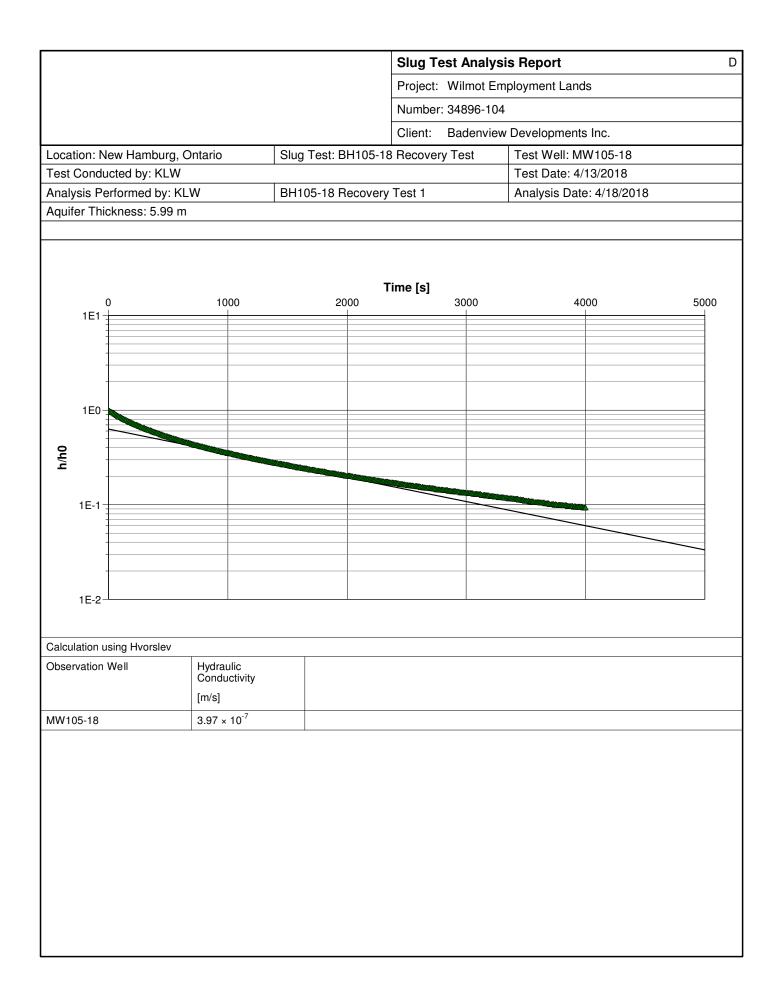
Drawing on experience...Building on

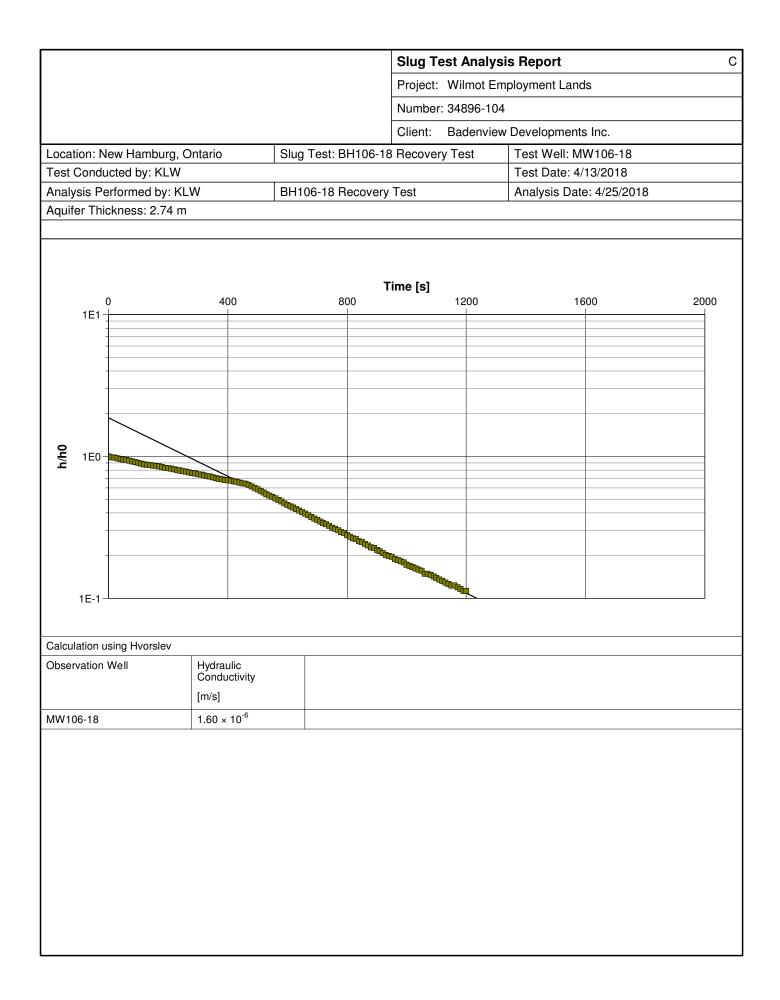
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						-						
					Slug Test Analysis Report D							
[Project: Wilmot Employment Lands							
[Number: 34896-104						
						Client: Badenview Developments Inc.						
Locatio	Location: New Hamburg, Ontario Slug Test: BH101-18						· · · · · · · · · · · · · · · · · · ·					
	Test Conducted by: KLW						Test Date: 4/13/2018					
	Analysis Performed by: KLW BH101-18 Recovery						Test Analysis Date: 4/18/2018					
Aquife	r Thic	kness: 2.61 m										
					г	ime [s]						
	0)	6000	1	2000	iiie [9]	18000	24	000	300	00	
	1E1+											
	+											
	1											
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Q		_										
0 4 /4	1E0-											
	-											
	+											
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	_											
	1E-1											
		sing Hvorslev	L Loulou a Pa									
Observ	ation v	vell	Hydraulic Conductivity									
			[m/s]									
MW101	MW101-18		4.60 × 10 ⁻⁸									

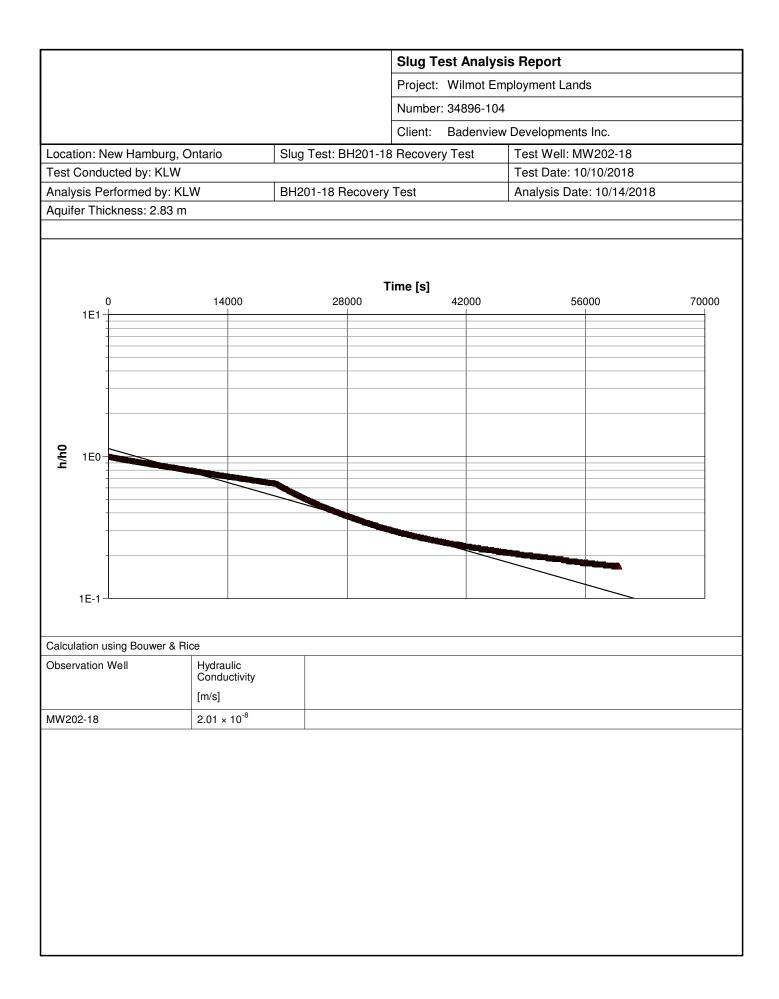


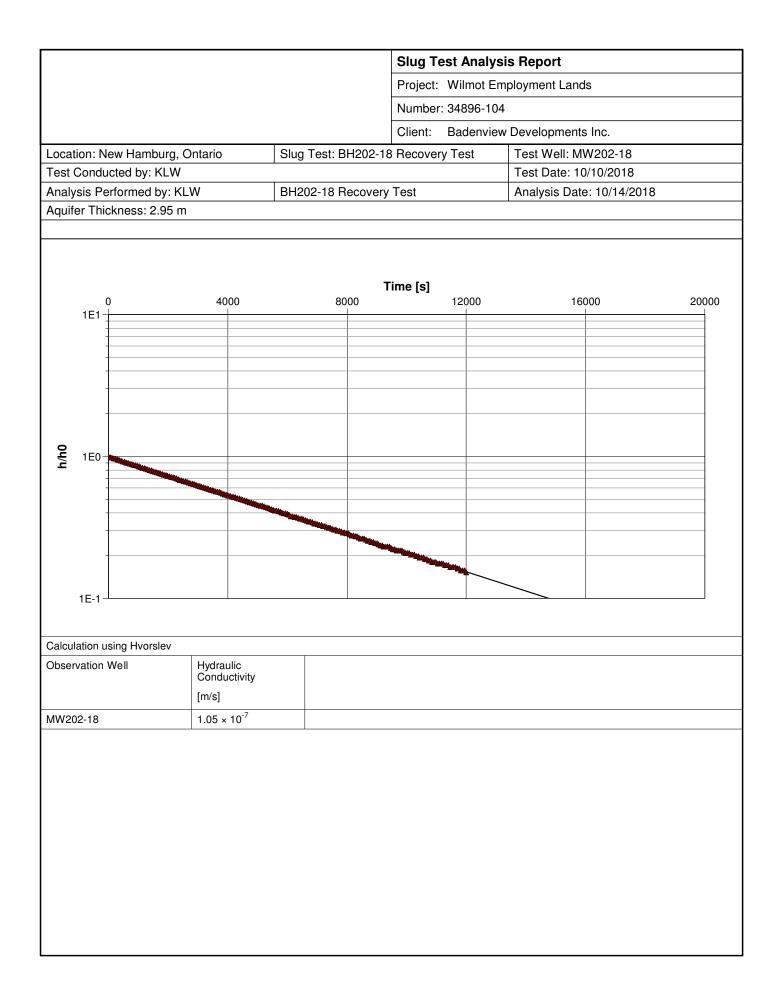
								<u> </u>				
						Slug Test Analysis Report D						
						Project: Wilmot Employment Lands						
						Number: 34896-104						
	Client: Badenview Developments Inc.											
Location: N	ew Hamburg, O	3 Recovery Test Test Well: MW104-18										
	icted by: KLW	I			Test Date: 4/13/2018							
Analysis Pe	erformed by: KL	W	BH104-18 R	{ecovery	Test							
Aquifer Thio	Aquifer Thickness: 9.07 m											
				-								
	0	6000	12	1 2000	ſime [s]	1800	0	24(000	300	000	
1E1-				+								
.												
.												
ع												
1E-1-												
	sing Hvorslev											
Observation		Hydraulic										
Observation	vven	Hydraulic Conductivity										
		[m/s]										
MW104-18		3.90 × 10 ⁻⁸										
			I									

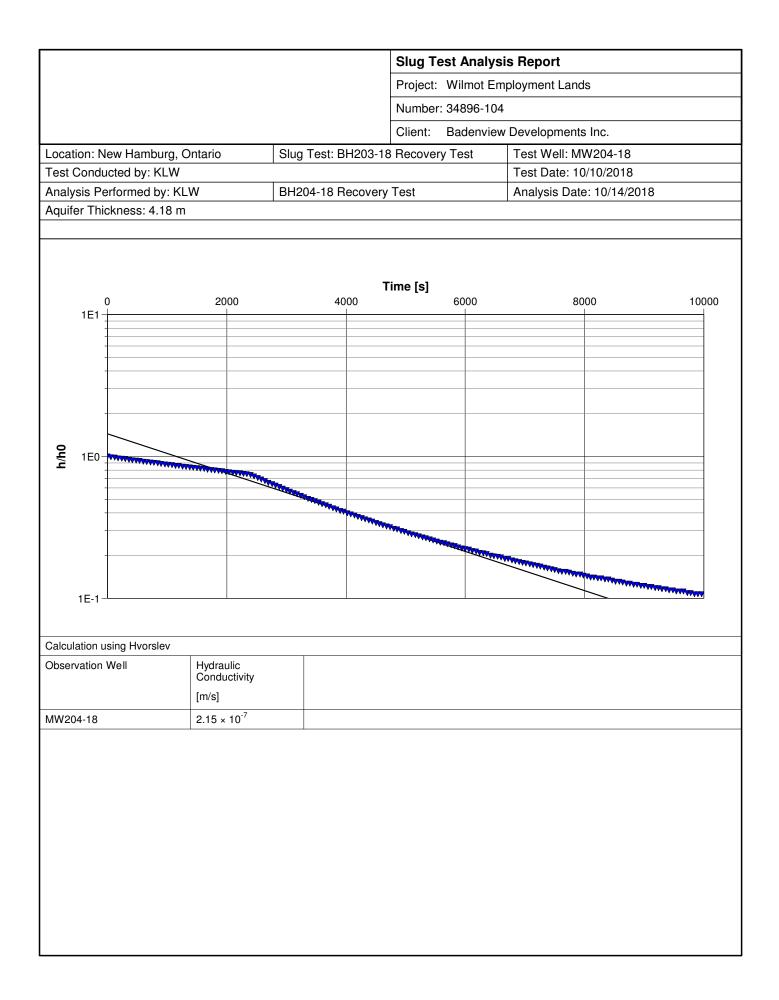




	Slug Test Analysis Report D									
	Project: Wilmot Employment Lands									
	Number: 34896-104									
				Client: Badenview Developments Inc.						
Location: New Hamburg, C	Jntario १	Slug Test: B	H107-18	Recovery Test Test Well: MW107-18						
Test Conducted by: KLW						Test Date: 4/13/2018				
Analysis Performed by: KL		3H107-18 R	ecovery	Test	Test Analysis Date: 4/18/2018					
Aquifer Thickness: 6.08 m										
Time [s]										
	6000	120	000		18000	24	000	3000	00	
1E1					_					
					_					
94 1E0										
							F			
1E-1										
Calculation using Hvorslev										
Observation Well	Hydraulic									
	Hydraulic Conductivity									
	[m/s]									
MW107-18	3.96 × 10 ⁻⁸									









APPENDIX E

GRAIN SIZE ANALYSIS

Drawing on experience...Building on

gth.

Peto MacCallum Ltd.

November 15, 2018

PML Ref.: 18KF009 Report: 2 (Revised)

Mr. Andrew Bingaman, C.E.T. MTE Consultants Inc. 520 Bingemans Centre Drive Kitchener, Ontario N2B 3X9

Dear Mr. Bingaman

Geotechnical Investigation Proposed Industrial Development Wilmot Employment Lands <u>New Hamburg, Ontario</u>

Please find enclosed the results of the particle size distribution analyses on samples submitted to our laboratory for the above referenced project.

Based on the laboratory test results and subsequent evaluation, the silt sample from Test Pit 1-18 would have an estimated hydraulic conductivity of 1×10^{-6} m/sec, and an infiltration rate of 10 mm/hour. The clayey silt sample from Test Pit 5-18 would have an estimated hydraulic conductivity of less than 1×10^{-8} m/sec, and an infiltration rate of less than 0.1 mm/hour.

We trust that the enclosed results are sufficient for your immediate needs. If you have any questions or require further information, please do not hesitate to contact our office.

Sincerely

Peto MacCallum Ltd.

William Loghrin, P.Eng. Project Engineer, Geotechnical Services

GM:sh

2 cc: MTE Consultants (+email) 1 cc: PML Kitchener

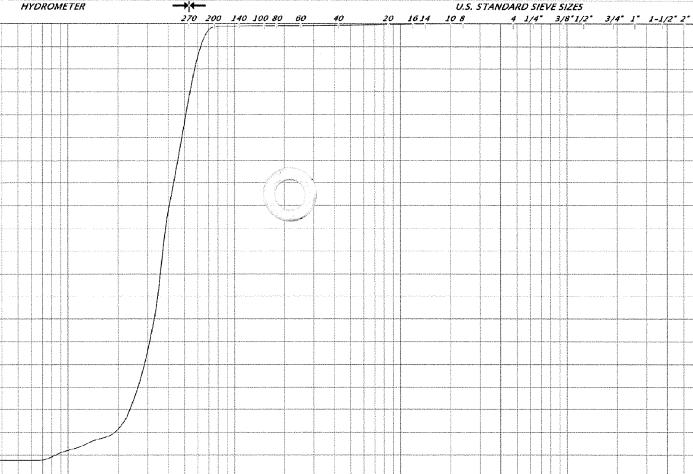
> 16 Franklin Street South, Kitchener, Ontario N2C 1R4 Tel: (519) 893-7500 Fax: (519) 893-0654 E-mail: kitchener@petomaccallum.com BARRIE, COLLINGWOOD, HAMILTON, KITCHENER, LONDON, TORONTO

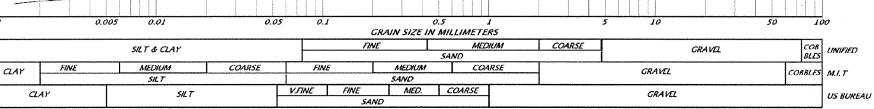


PROJECT NO. 18KF009 FIGURE NO. 1

3"

CUMULATIVE PERCENT RETAINED





REMARKS: Test Pit 1-18, Sample 1, Depth 4 m

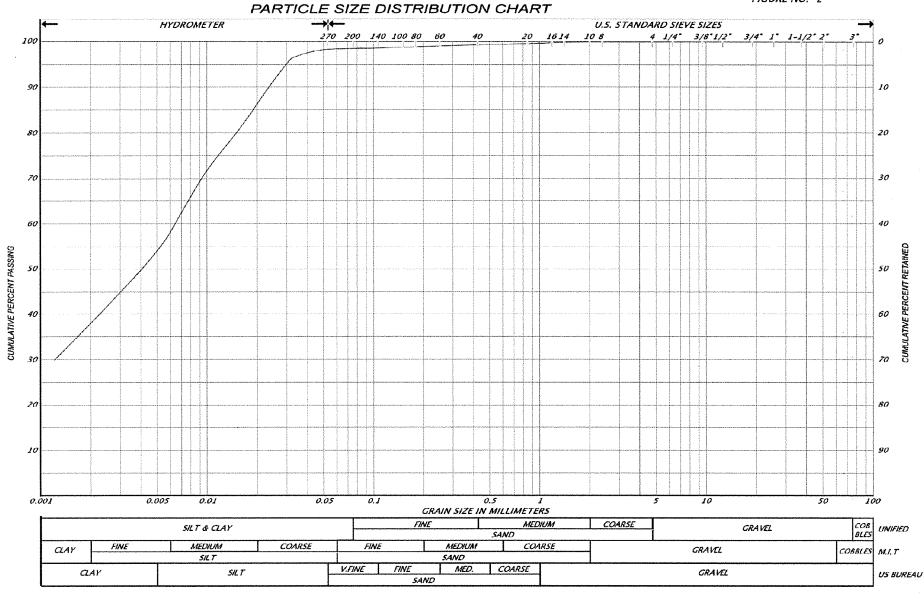
SILT

0.001

CUMULATIVE PERCENT PASSING



PROJECT NO. 18KF009 FIGURE NO. 2



REMARKS: Test Pit 5-18, Sample 1, Depth 4 m

CLAYEY SILT